

Annual Data Summary for 1994 CERC Field Research Facility

Volume I: Main Text and Appendixes A and B

by Michael W. Leffler, Clifford F. Baron, Brian L. Scarborough, Kent K. Hathaway, Paul R. Hodges, C. Ray Townsend

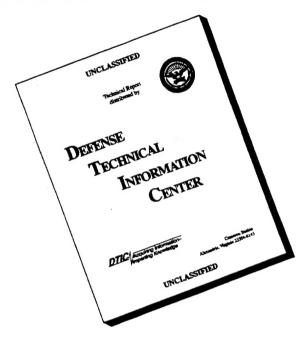
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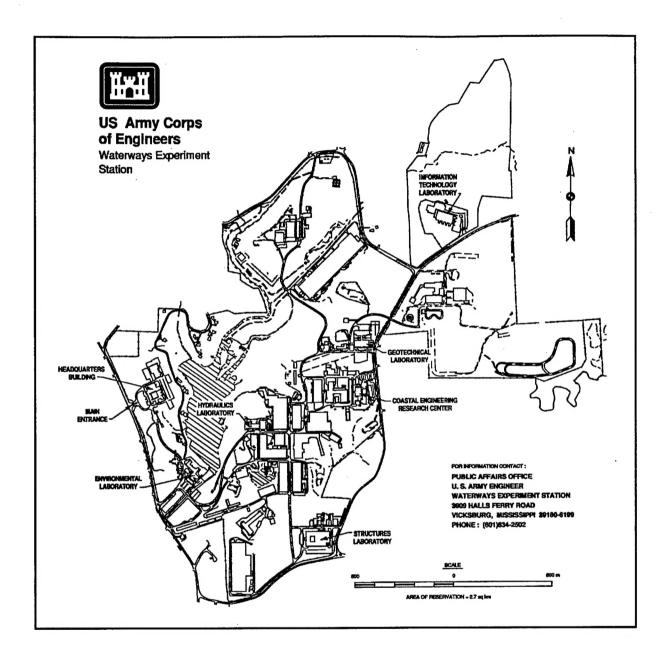
by Michael W. Leffler, Clifford F. Baron, Brian L. Scarborough, Kent K. Hathaway, Paul R. Hodges, C. Ray Townsend

U.S. Army Corps of Engineers Waterways Experiment Station 3909 Halls Ferry Road Vicksburg, MS 39180-6199

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¹ A limited number of copies of Appendixes C-E (Volume II) were published under separate cover. Copies are available from National Technical Information Service, 5285 Port Royal Road, Springfield, VA 22161.

Preface

This report is the 16th in a series of annual data summaries authorized by Headquarters, U.S. Army Corps of Engineers (HQUSACE), under Civil Works Research Work Unit 32525, "Field Research Facility Analysis," Coastal Flooding Program. Funds were provided through the U.S. Army Engineer Waterways Experiment Station (WES), Coastal Engineering Research Center (CERC), under the program management of Ms. Carolyn M. Holmes, CERC. The HQUSACE Technical Monitors were Messrs. John H. Lockhart, Jr., Barry W. Holliday, and Charles Chesnutt.

Data for the report were collected and analyzed at the WES/CERC Field Research Facility (FRF) in Duck, NC. The report was prepared by Mr. Michael W. Leffler, FRF, under the direct supervision of Mr. William A. Birkemeier, Chief, FRF Group, Engineering Development Division (EDD), and Mr. Thomas W. Richardson, Chief, EDD; and under the general supervision of Dr. James R. Houston and Mr. Charles C. Calhoun, Jr., Director and Assistant Director, CERC, respectively. Mr. Kent K. Hathaway, FRF, assisted with instrumentation. Mr. Brian L. Scarborough, FRF, and Messrs. William T. Lease, Mason O. Cox, Mark A. Lampe, Douglas A. Dorman, and Paul S. Magness assisted with data collection. Messrs. Clifford F. Baron and Guan-hong Lee, and Ms. Judy H. Roughton assisted with data analysis at the FRF. Additional assistance was provided by Ms. Dawn S. Miller, FRF. The National Oceanic and Atmospheric Administration/National Ocean Service maintained the tide gauge and provided statistics for summarization.

At the time of publication of this report, Director of WES was Dr. Robert W. Whalin. Commander was COL Bruce K. Howard, EN.

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1 Introduction

Background

The U.S. Army Engineer Waterways Experiment Station (WES), Coastal Engineering Research Center's (CERC's) Field Research Facility (FRF), located on 0.7 km² at Duck, NC (Figure 1), consists of a 561-m-long research pier and accompanying office and field support buildings. The FRF is located near the middle of Currituck Spit along a 100-km unbroken stretch of shoreline extending south of Rudee Inlet, VA, to Oregon Inlet, NC. The FRF is bordered by the Atlantic Ocean to the east and Currituck Sound to the west. The facility is designed to (a) provide a rigid platform from which waves, currents, water levels, and bottom elevations can be measured, especially during severe storms; (b) provide CERC with field experience and data to complement laboratory and analytical studies and numerical models; (c) provide a manned field facility for testing new instrumentation; and (d) serve as a permanent field base of operations for physical and biological studies of the site and adjacent region.

The research pier is a reinforced concrete structure supported on 0.9-m-diam steel piles spaced 12.2 m apart along the pier's length and 4.6 m apart across the width. The piles are embedded approximately 20 m below the ocean bottom. The pier deck is 6.1 m wide and extends from behind the duneline to about the 6-m water depth contour at a height of 7.8 m above the National Geodetic Vertical Datum (NGVD). The pilings are protected against sand abrasion by concrete erosion collars and against corrosion by a cathodic system.

An FRF Measurements and Analysis Program has been established to collect basic oceanographic and meteorological data at the site, reduce and analyze these data, and publish the results.

This report, which summarizes data for 1994, continues a series of reports begun in 1977.

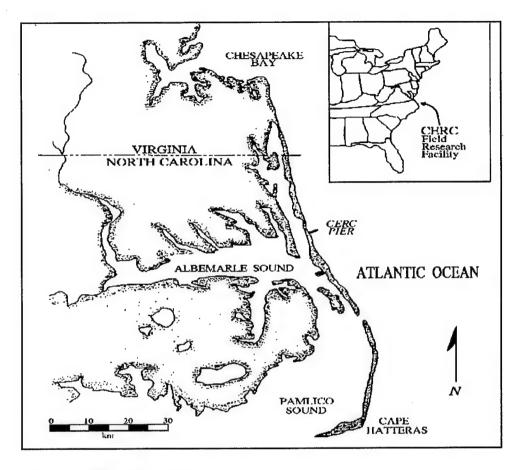


Figure 1. FRF location map

Organization of Report

This report is organized into nine chapters and five appendixes. Chapter 1 is an introduction; Chapters 2 through 8 discuss the various data collected during the year; and Chapter 9 describes the storms that occurred. Appendix A presents the bathymetric surveys, Appendix B summarizes deepwater wave statistics, and Appendixes C through E (published under separate cover as Volume II) contain summary statistics for other gauges.

In each chapter of this report, the respective instruments used for monitoring the meteorological or oceanographic conditions are briefly described, along with data collection and analysis procedures and data results. The instruments were interfaced with the primary data acquisition system, a Digital Equipment Corporation (Maynard, MA) VAX-11/750 minicomputer until June when it was replaced with a Digital Equipment Corporation VAXstation 4000 located in the FRF laboratory building. More detailed explanations of the design and the operation of the instruments may be found in Miller (1980). Readers' comments on the format and usefulness of the data presented are encouraged.

Availability of Data

Table 1 summarizes the available data. In addition to the wave data summaries in the main text, more extensive summaries for each of the wave gauges are provided in Appendixes B through E.

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Beach															,	4	,													•				•-						-	-	-	•

The annual data summary herein summarizes daily observations by month and year to provide basic data for analysis by users. Daily measurements and observations have already been reported in a series of monthly Preliminary Data Summaries (FRF 1994). If individual data for the present year are needed, the user can obtain detailed information (as well as the monthly and previous annual reports) from the following address:

USAE Waterways Experiment Station Coastal Engineering Research Center Field Research Facility 1261 Duck Rd. Kitty Hawk, NC 27949-4472 Although the data collected at the FRF are designed primarily to support ongoing CERC research, use of the data by others is encouraged. Tidal data other than the summaries in this report can be obtained directly from the following address:

National Oceanic and Atmospheric Administration National Ocean Service ATTN: Tide Analysis Branch Rockville, MD 20852

A complete explanation of the exact data desired for specific dates and times will expedite filling any request; an explanation of how the data will be used will help CERC or the National Oceanic and Atmospheric Administration (NOAA)/National Ocean Service (NOS) determine whether other relevant data are available. For information regarding the availability of data for all years, contact the FRF at (919) 261-3511. Costs for collecting, copying, and mailing will be borne by the requester.

2 Meteorology

This chapter summarizes the meteorological measurements made during the current year and in combination with all previous years. Meteorological measurements during storms are given in Chapter 9.

Mean air temperature, atmospheric pressure, and wind speed and direction were computed for each data file, which consisted of data sampled two times per second for 34 min every 6 hr beginning at or about 0100, 0700, 1300, and 1900 hr eastern standard time (EST); these hours correspond to the time that the National Weather Service (NWS) creates daily synoptic weather maps. During storms, data recordings were made more frequently. Meteorological data are summarized in Table 2.

		Mean	Me	ean						Wind Re	sul tant	s
		emperature		meric Pres.		recipit	ation, i	m		1994	198	0-1994
		deg C		шp	1994		1978-19		Speed	Direction	Speed	Direction
<u>Month</u>	1994	1983-1994	1994	<u> 1983-1994</u>	<u>Total</u>	Mean	Maxima	Minima	m/sec	deg	m/sec	deg
Jan	3.4	6.2	1021.3	1017.9	182	112	210	44	2.8	322	2.3	332
Feb	5.3	6.7	1021.7	1017.4	85	71	113	20	1.5	326	1.9	344
Mar	10.2	9.5	1013.8	1015.9	231	110	231	3 5	0.9	249	1.2	350
Apr	16.9	13.9	1018.7	1014.4	98	93	182	0	1.7	198	0.2	308
May	17.7	18.6	1014.6	1015.7	159	76	239	20	1.7	0	0.2	153
Jun	24.7	23.7	1014.8	1015.1	90	88	136	27	2.7	183	1.1	189
Jul	27.0	26.5	1017.1	1015.9	<i>7</i> 5	97	275	19	4.0	203	2.1	208
Aug	24.2	25.5	1017.6	1016.3	191	110	253	30	0.5	208	0.5	106
Sep	21.9	22.8	1016.1	1017.6	136	81	226	5	1.1	8	1.8	39
0ct	17.3	17.9	1016.1	1018.6	102	75	143	17	4.2	23	2.4	26
Nov	14.8	13.6	1017.9	1018.4	129	90	145	26	2.1	346	1.7	347
Dec	10.7	8.2	1019.8	1019.2	109	68	131	4	4.9	359	2.4	331
Average Total	16.2	16.1	1017.5	1016.8	132 1587	89 1071			0.8	331	0.8	351

Air Temperature

The FRF enjoys a typical marine climate that moderates the temperature extremes of both summer and winter.

Measurement instruments

A Yellow Springs Instrument Company, Inc. (YSI) (Yellow Springs, OH), electronic temperature probe with analog output interfaced to the FRF's computer was operated beside the NWS's meteorological instrument shelter located 43 m behind the dune (Figure 2). To ensure proper temperature readings,

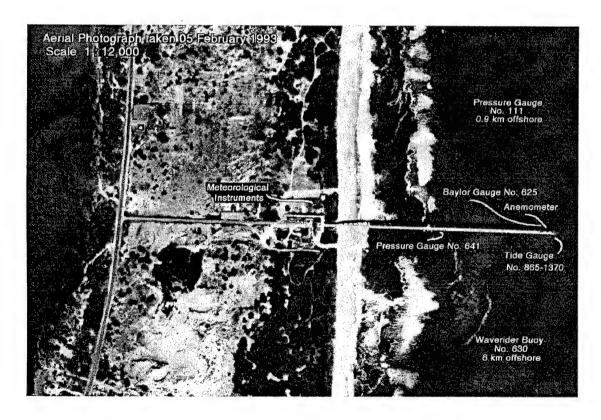


Figure 2. FRF gauge locations

the probe was installed 3 m above ground inside a "coolie hat" to shade it from direct sun, yet provide proper ventilation.

Results

Daily and average air temperature values are tabulated in Table 2 and shown in Figure 3.

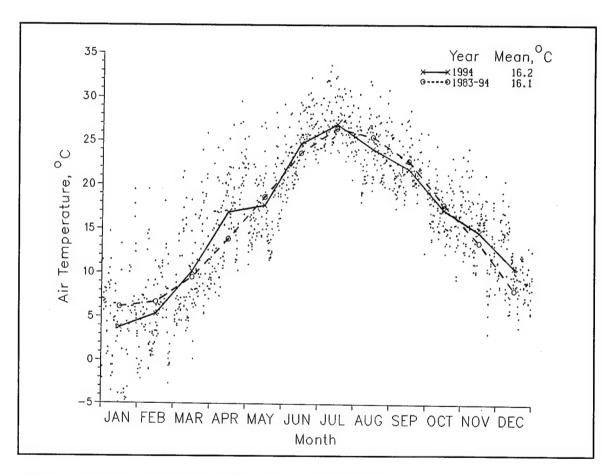


Figure 3. Daily air temperature values with monthly means

Atmospheric Pressure

Measurement instruments

Electronic atmospheric pressure sensor. Atmospheric pressure was measured with a YSI electronic sensor with analog output located in the laboratory building at 9 m above NGVD. Data were recorded on the FRF computer. Data from this gauge were compared with those from an NWS aneroid barometer to ensure proper operation.

Microbarograph. A Weathertronics, Incorporated (Sacramento, CA), recording aneroid sensor (microbarograph) located in the laboratory building was also used to continuously record atmospheric pressure variation.

The microbarograph was compared daily with the NWS aneroid barometer, and adjustments were made as necessary. Maintenance of the microbarograph consisted of inking the pen, changing the chart paper, and winding the clock every 7 days. During the summer, a meteorologist from the NWS checked and verified the operation of the barometer.

The microbarograph was read and inspected daily using the following procedure:

- a. The pen was zeroed (where applicable).
- b. The chart time was checked and corrected, if necessary.
- c. The daily reading was marked on the chart for reference.
- d. The starting and ending chart times were recorded, as necessary.
- e. New charts were installed, when needed.

Results

Daily and average atmospheric pressure values are presented in Figure 4, and summary statistics are presented in Table 2.

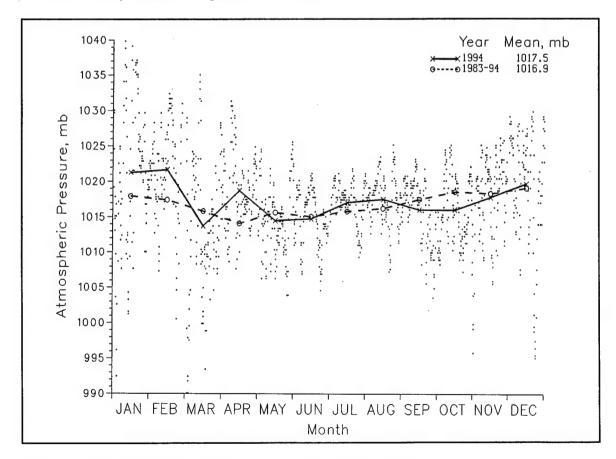


Figure 4. Daily barometric pressure values with monthly means

Precipitation

Precipitation is generally well distributed throughout the year. Precipitation from mid-latitude cyclones (northeasters) predominates in the winter, whereas local convection (thunderstorms) accounts for most of the summer rainfall.

Measurement instruments

Electronic rain gauge. A Belfort Instrument Company (Baltimore, MD) 30-cm weighing rain gauge, located near the instrument shelter 47 m behind the dune, measured daily precipitation. According to the manufacturer, the instrument's accuracy was 0.5 percent for precipitation amounts less than 15 cm and 1.0 percent for amounts greater than 15 cm.

The rain gauge was inspected daily; however, the analog chart recorder was inoperable the entire year.

Plastic rain gauge. An Edwards Manufacturing Company (Alberta Lea, MN) True Check 15-cm-capacity clear plastic rain gauge with a 0.025-cm resolution was used to monitor the performance of the weighing rain gauge. This gauge was located near the weighing gauge, and the gauges were compared on a daily basis. Very few discrepancies were identified during the year.

Results

Daily and monthly average precipitation values are shown in Figure 5. Statistics of total precipitation for each month during this year and average totals for all years combined are presented in Table 2.

Wind Speed and Direction

Winds at the FRF are dominated by tropical maritime air masses that create low to moderate, warm southern breezes; arctic and polar air masses that produce cold winds from northerly directions; and smaller scale cyclonic, low pressure systems, which originate either in the tropics (and move north along the coast) or on land (and move eastward offshore). The dominant wind direction changes with the season, being generally from northern directions in the fall and winter and from southern directions in the spring and

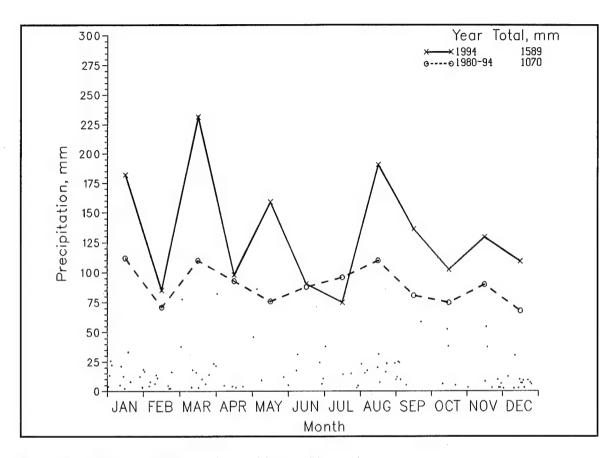


Figure 5. Daily precipitation values with monthly totals

summer. It is common for fall and winter storms (northeasters) to produce winds with average speeds in excess of 15 m/sec.

Measurement instrument

Winds were measured at the seaward end of the pier at an elevation of 19.1 m (Figure 2) using a Weather Measure Corporation (Sacramento, CA) Skyvane Model W102P anemometer. Wind speed and direction data were collected on the FRF computer. The anemometer manufacturer specifies an accuracy of ± 0.45 m/sec below 13 m/sec and 3 percent at speeds above 13 m/sec, with a threshold of 0.9 m/sec. Wind direction accuracy is ± 2 deg, with a resolution of less than 1 deg. The anemometer is calibrated annually at the National Bureau of Standards in Gaithersburg, MD, and is within the manufacturer's specifications.

Results

Annual and monthly joint probability distributions of wind speed versus direction were computed. Wind speeds were resolved into 3-m/sec intervals, whereas the directions were at 22.5-deg intervals (i.e., 16-point compass direction specifications). These distributions are presented as wind "roses," such that the length of the petal represents the frequency of occurrence of wind blowing from the specified direction, and the width of the petal is indicative of the speed. Resultant directions and speeds were also determined by vector-averaging the data (see Table 2). Wind statistics are presented in Figures 6-8.

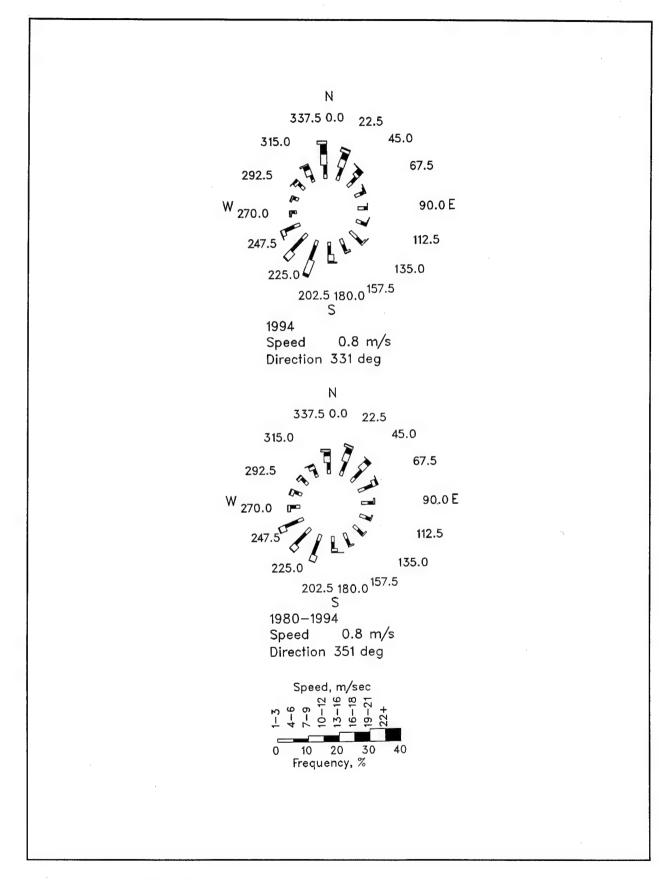


Figure 6. Annual wind roses

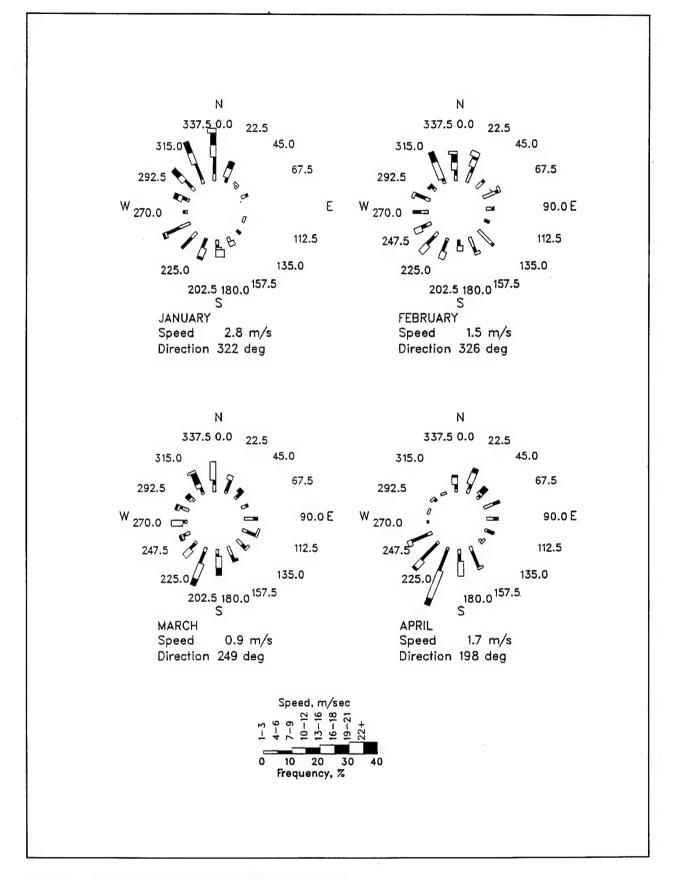


Figure 7. Monthly wind roses for 1994 (Continued)

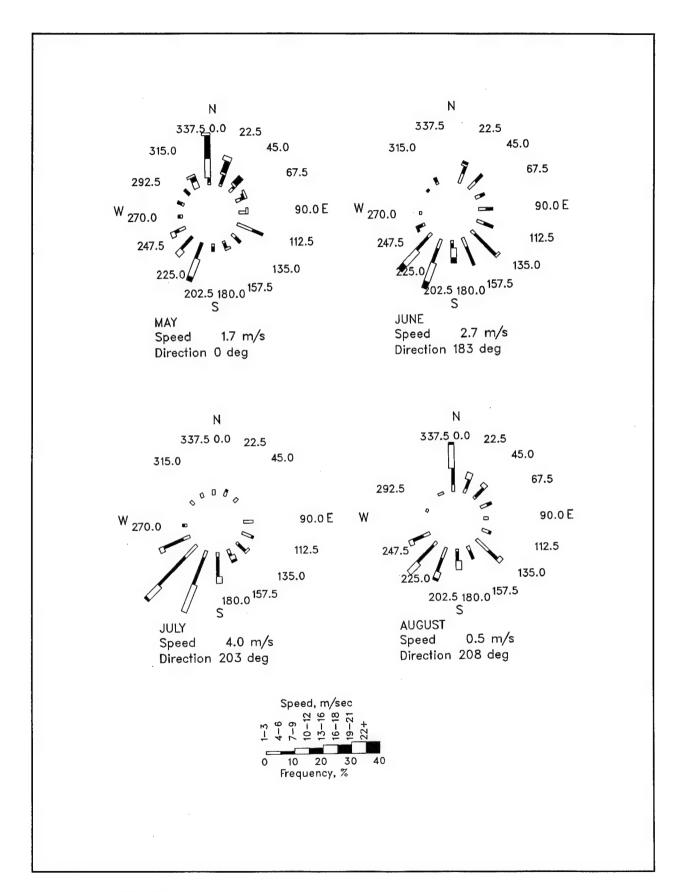


Figure 7. (Continued)

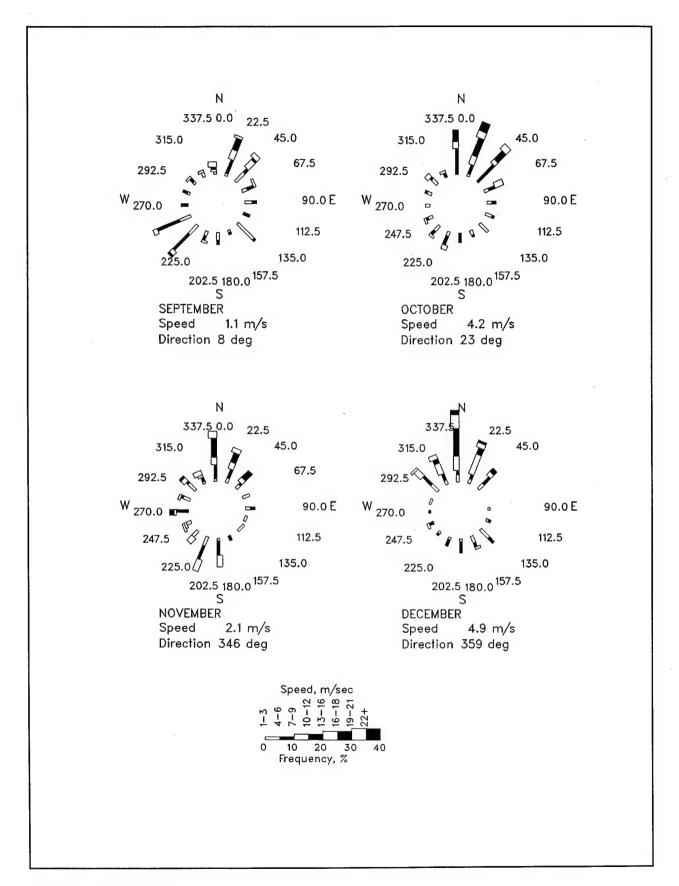


Figure 7. (Concluded)

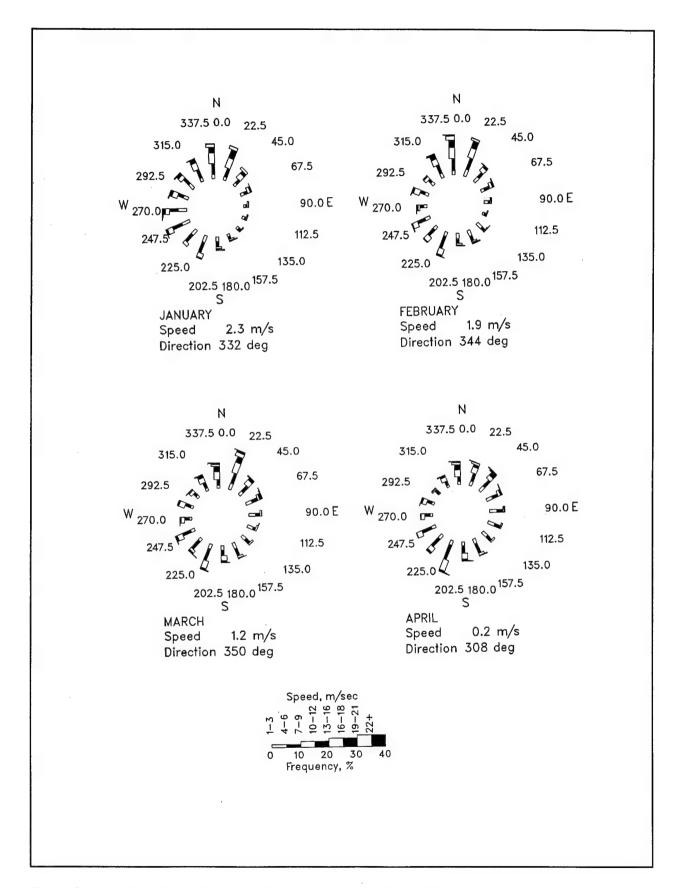


Figure 8. Monthly wind roses for 1980 through 1994 (Continued)

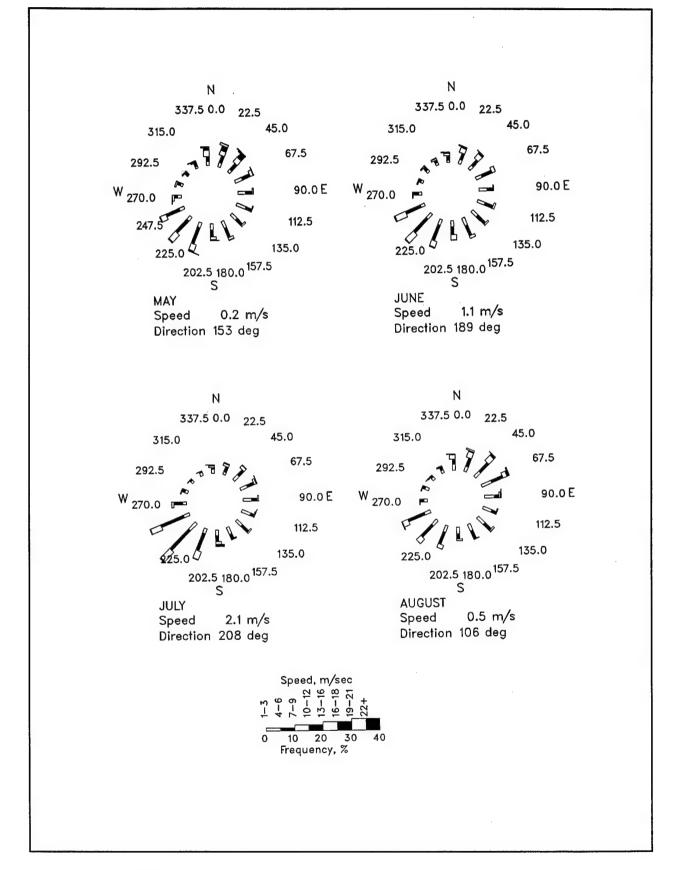


Figure 8. (Continued)

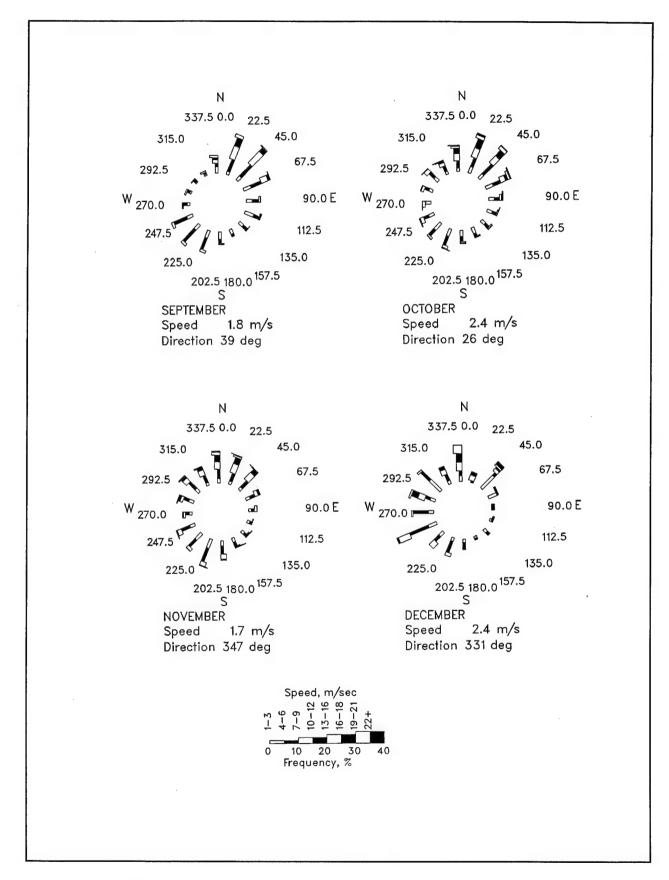


Figure 8. (Concluded)

3 Waves

This chapter presents summaries of the wave data. A discussion of individual major storms is given in Chapter 9 and contains additional wave data for times when wave heights exceeded 2 m at the seaward end of the FRF pier. Appendixes B through E provide more extensive data summaries for each gauge, including height and period distributions, wave direction distributions, persistence tables, and spectra during storms.

Wave directions (similar to wind directions) at the FRF are seasonally distributed. Waves approach most frequently from north of the pier in the fall and winter and south of the pier in the summer, with the exception of storm waves that approach twice as frequently from north of the pier. Annually, waves are approximately evenly distributed between north and south (resultant wave direction being almost shore-normal).

Measurement Instruments

The wave gauges included one wave staff gauge (Gauge 625), one buoy gauge (Gauge 630), and two pressure gauges (Gauges 111 and 641) as shown in Figure 2. Staff gauge 645 failed in May 1992 and was replaced by pressure gauge 641 at the same location. The gauges were located as follows:

Gauge Type/Number Continuous wire (645)	Distance Offshore <u>from Baseline</u> 238 m	Water Depth m 3.5	Operationa Period
Pressure Gauge (641)	238 m	3.5	11/84-05/92 11/92-12/94
Continuous wire (625) Accelerometer buoy (630)	567 m 6 km	8 18	11/78-12/94 11/78-12/94
Pressure gauge (111)	1 km	8	09/86-12/94

Staff gauges

One Baylor Company (Houston, TX) parallel cable inductance wave gauge (Gauge 625 at sta 18+60 (Figure 2)) was mounted on the FRF pier. Rugged and reliable, this gauge requires little maintenance except to keep tension on the cables and to remove any material that may cause an electrical

short between them. It was calibrated prior to installation by creating an electrical short between the two cables at known distances along the cable and recording the voltage output. Electronic signal conditioning amplifiers are used to ensure that the output signals from the gauge are within a 0- to 5-V range. Manufacturer-stated gauge accuracy is about 1.0 percent, with a 0.1-percent full-scale resolution; full scale is 14 m for Gauge 625. This gauge is susceptible to lightning damage, but protective measures have been taken to minimize such occurrences. A more complete description of the gauges' operational characteristics is given by Grogg (1986).

Buoy gauge

One Datawell Laboratory for Instrumentation (Haarlem, The Netherlands), Waverider buoy gauge (Gauge 630) measures the vertical acceleration produced by the passage of a wave. The acceleration signal is double-integrated to produce a displacement signal transmitted by radio to an onshore receiver. The manufacturer stated that wave amplitudes are correct to within 3 percent of their actual value for wave frequencies between 0.065 and 0.500 Hz (corresponding to 15- to 2-sec wave periods). The manufacturer also specified that the error gradually increased to 10 percent for wave periods in excess of 20 sec. The results in this report were not corrected for the manufacturer's specified amplitude errors. However, the buoy was calibrated semiannually to ensure that it was within the manufacturer's specification.

Pressure gauges

One Senso-Metrics, Incorporated (Simi Valley, CA), pressure transduction gauge (Gauge 111) installed near the ocean bottom measures the pressure changes produced by the passage of waves creating an output signal that is linear and proportional to pressure when operated within its design limits. Predeployment and postdeployment calibrations are performed at the FRF using a static deadweight tester. The sensor's range is 0 to 25 psi (equivalent to 0 to 17 m of seawater) above atmospheric pressure with a manufacturer-stated accuracy of ± 0.25 percent. Copper scouring pads are installed at the sensor's diaphragm to reduce biological fouling, and the system is periodically cleaned by divers.

One Paroscientific, Incorporated (Redmond, WA), pressure transduction gauge (Gauge 641) was installed near the ocean bottom on an instrument pile under the pier at station 7+80. Calibration is similar to that performed on Gauge 111. The sensor's range is 0 to 45 psia (equivalent to 0 to 30 m of seawater) with a manufacturer-stated accuracy of ± 0.01 percent. A perforated copper/nickel plate protects the sensor's diaphragm from biological fouling, and the system is periodically cleaned by divers.

Digital Data Analysis and Summarization

The data were collected, analyzed, and then archived on optical disk using the FRF's VAX computer. Data sets were normally collected every 3 hr. For each gauge, a data set consisted of five contiguous records of 4,096 points recorded at 0.5 Hz (approximately 34-min long), for a total of 2 hr and 50 minutes, resulting in only a 10-min gap between data sets. Analysis was performed on individual 34-min records.

The analysis program computes the first moment (mean) and the second moment about the mean (variance) and then edits the data by checking for "jumps," "spikes," and points exceeding the voltage limit of the gauge. A jump is defined as a data value greater than five standard deviations from the previous data value, whereas a spike is a data value more than five standard deviations from the mean. If less than five consecutive jumps or spikes are found, the program linearly interpolates between acceptable data and replaces the erroneous data values. The editing stops if the program finds more than five consecutive jumps or spikes, or more than a total of 100 bad points, or the variance of the voltage is below 1×10^{-5} squared volts. The statistics and diagnostics from the analysis are saved.

Sea surface energy spectra are computed from the edited time series. Spectral estimates are computed from smaller data segments obtained by dividing the 4,096-point record into several 512-point segments. The estimates are then ensemble-averaged to produce a more accurate spectrum. These data segments are overlapped by 50 percent (known as the Welch (1967) method) which has been shown to produce better statistical properties than nonoverlapped segments. The mean and linear trends are removed from each segment prior to spectral analysis. To reduce side-lobe leakage in the spectral estimates, a data window was applied. The first and last 10 percent of data points were multiplied by a cosine bell (Bingham, Godfrey, and Tukey 1967). Spectra were computed from each segment with a discrete Fast Fourier Transform and then ensemble-averaged. Sea surface spectra from subsurface pressure gauges were obtained by applying the linear wave theory transfer function.

Unless otherwise stated, wave height in this report refers to the energy-based parameter H_{mo} defined as four times the zeroth moment wave height of the estimated sea surface spectrum (i.e., four times the square root of the variance) computed from the spectrum passband. Energy computations from the spectra are limited to a passband between 0.05 and 0.50 Hz for surface gauges and between 0.05 Hz and a high-frequency cutoff for subsurface gauges. This high-frequency limit is imposed to eliminate aliased energy and noise measurements from biasing the computation of H_{mo} and is defined as the frequency where the linear theory transfer function is less than 0.1 (spectral values are multiplied by 100 or more). Smoother and more statistically significant spectral estimates are obtained by band-averaging contiguous spectral components (three components are averaged per band, producing a frequency band width of 0.0117 Hz).

Wave period T_p is defined as the period associated with the maximum energy band in the spectrum, which is computed using a 3-point running average band on the spectrum. The peak period is reported as the reciprocal of the center frequency (i.e., $T_p = 1/\text{frequency}$) of the spectral band with the highest energy. A detailed description of the analysis techniques is presented in Andrews (1987).²

Results

The wave conditions for the year are shown in Figure 9. For all four gauges, the distributions of wave height for the current year and all years combined are presented in Figures 10 and 11, respectively. Distributions of wave period are presented in Figure 12.

Multiple-year comparisons of data for Gauge 111 actually incorporate data for 1985 and 1986 from Gauge 640 (a discontinued Waverider buoy previously located at the approximate depth and distance offshore of Gauge 111) and data for 1987 from Gauge 141, located 30 m south of Gauge 111. In addition Gauge 511 was used from January through October 1993. Multiple-year data for Gauge 641 also include data from Gauge 645 (a Baylor staff gauge) which was mounted at the same location as Gauge 641 from November 1984 until May 1992, when it failed.

Refraction, bottom friction, and wave breaking contribute to the observed differences in height and period. During the most severe storms when the wave heights exceed 3 m at the seaward end of the pier, the surf zone (wave breaking) has been observed to extend past the end of the pier and occasionally 1 km offshore. This occurrence is a major reason for the differences in the distributions between Gauge 630 and the inshore gauges. The wave height statistics for the pressure gauge (Gauge 641), located at the landward end of the pier, were considerably lower than those for the other gauges. In all but the calmest conditions, this gauge is within the breaker zone. Consequently, these statistics represent a lower energy wave climate.

² M. E. Andrews. 1987. "Standard wave data analysis procedures for coastal engineering applications," unpublished report prepared for U.S. Army Engineer Waterways Experiment Station, Vicksburg, MS.

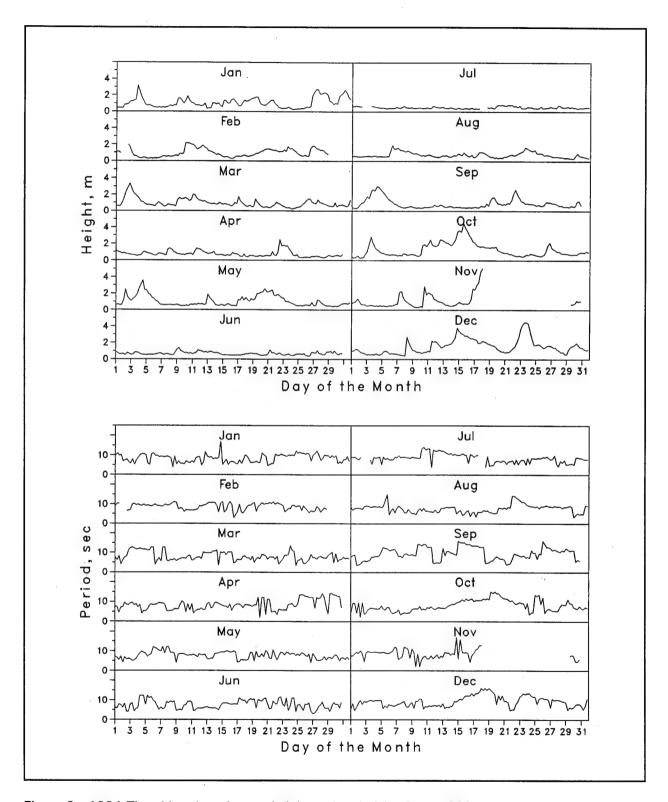


Figure 9. 1994 Time-histories of wave height and period for Gauge 630

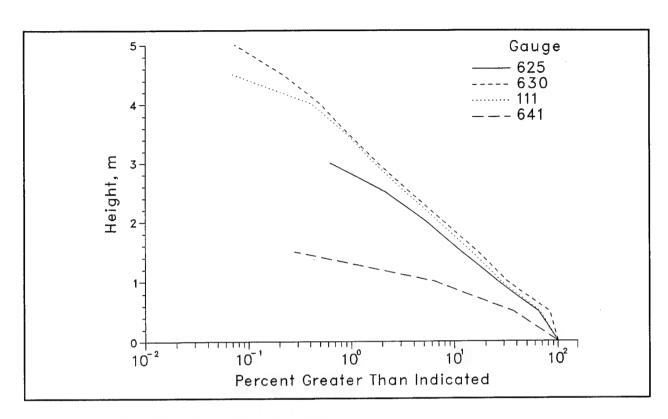


Figure 10. 1994 annual wave height distributions

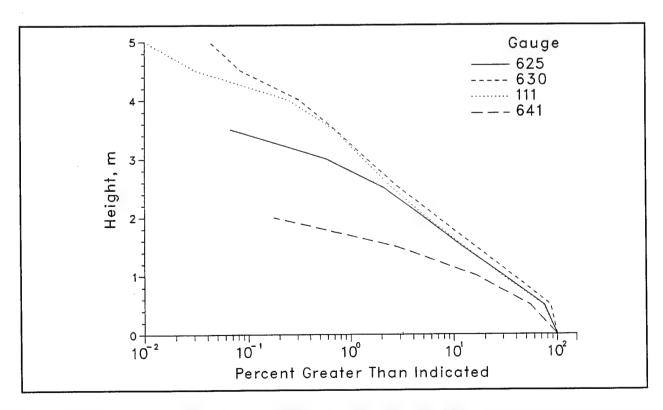


Figure 11. Annual distribution of wave heights for 1980 through 1994

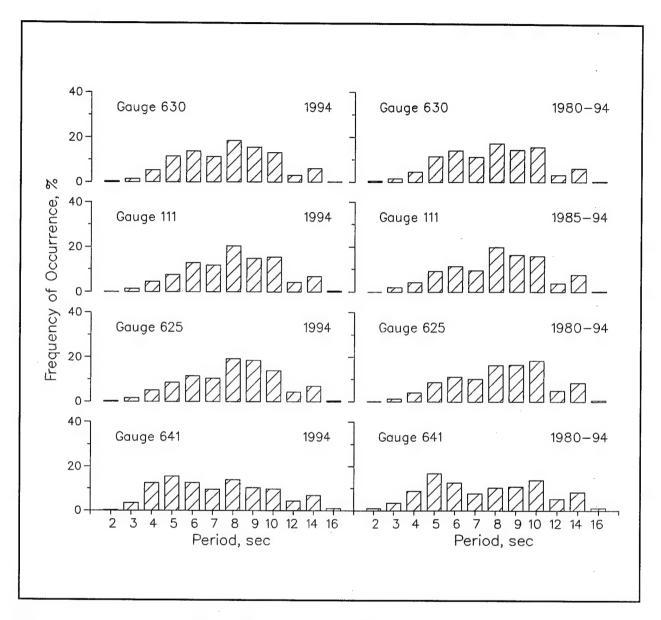


Figure 12. Annual wave period distributions for all gauges

Summary wave statistics for the current year and all years combined are presented for Gauge 630 in Table 3.

Table 3
Wave Statistics for Gauge 630

				1994				1980-1994										
		Hei	ght	1,,,,	Per	iod			Hei	ght		Per	iod					
		Std.				Std.			Std.				Std.					
	Mean	Dev.	Extreme		Mean	Dev.	Number	Mean	Dev.	Extreme		Mean	Dev.	Number				
<u>Month</u>	· m	<u>m</u>	m	<u>Date</u>	sec	sec	Obs.	m	m	m	Date	sec	sec	Obs.				
Jan	1.1	0.7	3.2	3	8.4	2.2	122	1.2	0.7	4.5	1983	8.1	2.6	1496				
Feb	1.0	0.6	2.2	10	8.6	1.8	109	1.2	0.7	5.1	1987	8.4	2.5	1352				
Mar	1.0	0.6	3.3	2	8.0	2.4	123	1.2	0.7	4.7	1983	8.6	2.6	1691				
Apr	0.8	0.4	2.5	22	8.4	2.7	118	1.0	0.6	5.0	1988	8.6	2.7	1670				
May	1.1	0.7	3.6	4	7.8	1.9	124	0.9	0.5	3.6	1992	8.2	2.4	1713				
Jun	0.7	0.2	1.4	9	7.7	2.3	119	0.8	0.4	2.7	1991	7.9	2.2	1597				
Jul	0.6	0.2	0.8	20	8.5	2.3	116	0.7	0.3	2.1	1985	8.0	2.4	1629				
Aug	0.8	0.4	1.9	6	7.6	2.1	121	0.8	0.4	3.6	1981	8.1	2.4	1655				
Sep	1.0	0.7	3.0	4	9.5	3.2	120	1.0	0.6	6.1	1985	8.6	2.6	1654				
Oct	1.3	0.9	4.5	15	8.1	2.9	124	1.3	0.8	5.4	1991	8.7	2.8	1729				
Nov	1.1	1.0	5.1	18	8.6	2.6	75	1.2	0.7	5.1	1994	8.0	2.7	1470				
Dec	1.6	1.0	4.5	23	9.3	2.8	123	1.3	0.8	5.6	1980	8.4	2.9	1475				
Annual	1.0	0.7	5.1	Nov	8.4	2.5	1394	1.0	0.7	6.1	Sep 1985	8.3	2.6	19131				
Armuat	1.0	0.7	J. 1	NOV	0.4		1371											

Annual joint distributions of wave height versus wave period for Gauge 630 are presented for 1994 in Table 4, and for all years combined in Table 5. Similar distributions for the other gauges are included in Appendixes B-E.

Annual distributions of wave directions (relative to true north) based on daily observations of direction at the seaward end of the pier and height from Gauge 625 (or Gauge 111 when data for Gauge 625 were unavailable) are shown in Figure 13. Monthly wave roses for 1994 and all years combined are presented in Figures 14 and 15, respectively.

Table 4 Annual (1994) Joint Distribution of H_{mo} versus T_p for Gauge 630 1

						Peri	od, se	c					
	2.0-	3.0-	4.0-	5.0-	6.0-	7.0-	8.0-	9.0-	10.0-	12.0-	14.0-	16.0-	
Height, m	2.9	<u>3.9</u>	4.9	5.9	6.9	7.9	8.9	9.9	11.9	13.9	15.9	Longer	Total
0.00 - 0.49	29	14	22	65	43	115	459	416	244	158	108		1673
0.50 - 0.99	7	108	359	502	667	617	1055	861	581	57	273	14	5101
1.00 - 1.49		22	151	395	237	151	187	158	194	22	57		1574
1.50 - 1.99				172	273	115	57	36	136	29	57		875
2.00 - 2.49				14	143	86	36	29	50	7	50		415
2.50 - 2.99		-		•	14	50	36	22	22	7	36		187
3.00 - 3.49	•					7	7	14	50	7			85
3.50 - 3.99			•					22	22				44
4.00 - 4.49									7	14	7		28
4.50 - 4.99											14		14
5.00 - Greater	•		•								7		7
Total	36	144	532	1148	1377	1141	1837	1558	1306	301	609	14	

¹ Percent occurrence (x100) of height and period.

Table 5 Annual (1980-1994) Joint Distribution of H_{mo} versus T_p for Gauge 630 (All Years) 1

						Pe	riod,	sec				•	
	2.0-	3.0-	4.0-	5.0-	6.0-	7.0-	8.0-	9.0-	10.0-	12.0-	14.0-	16.0-	-
<u> Keight, m</u>	2.9	<u> </u>	4.9	5.9	6.9	7.9	8.9	9.9	11.9	13.9	15.9	Longer	Total
		·											
0.00 - 0.49	25	15	28	63	80	123	356	293	194	68	119	4	1368
0.50 - 0.99	32	135	271	490	570	536	915	773	764	125	225	14	4850
1.00 - 1.49		10	147	405	404	237	274	216	318	39	112	3	2165
1.50 - 1.99			11	166	244	106	82	76	137	32	66	3	923
2.00 - 2.49			1	25	93	68	52	33	62	26	34	1	395
2.50 - 2.99				1	14	34	20	15	34	9	25	i	153
3.00 - 3.49					1	11	13	13	21	6	8	i	74
3.50 - 3.99						1	6	9	13	5	5	'	. 39
4.00 - 4.49				-			3	5	.8	3	4	i	24
4.50 - 4.99			_	_		-	_	1	5	-	1	1	5
5.00 - Greater		-	-	-			i		1	1	1	1	[]
Total	57	160	458	1150	1406	1116	1722	1434	1554	314	600	30	ر
Totat		100	470	1130	1400	1110	1122	1434	1004	514	600	30	

¹ Percent occurrence (x100) of height and period.

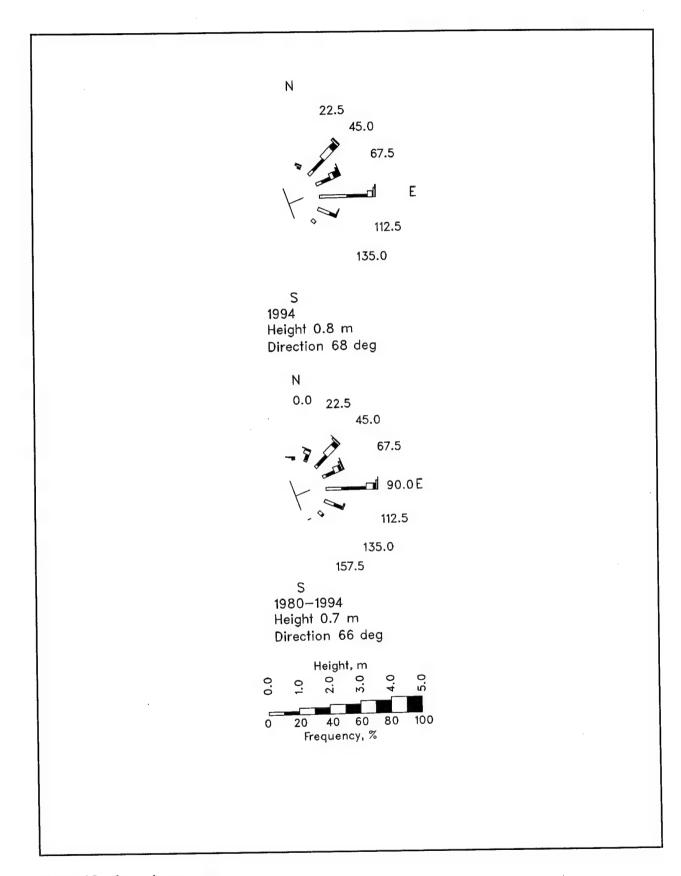


Figure 13. Annual wave roses

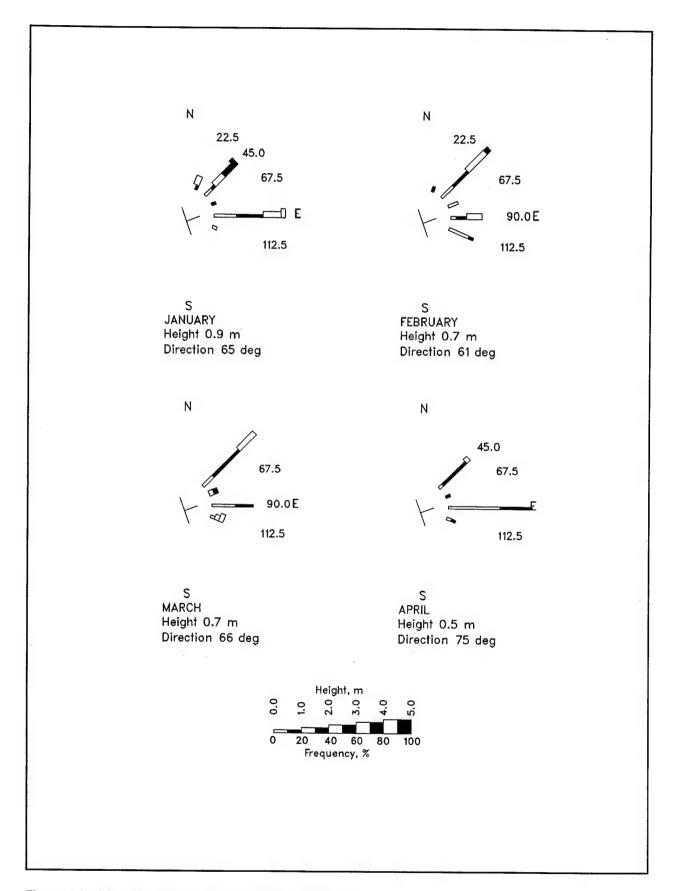


Figure 14. Monthly wave roses for 1994 (Continued)

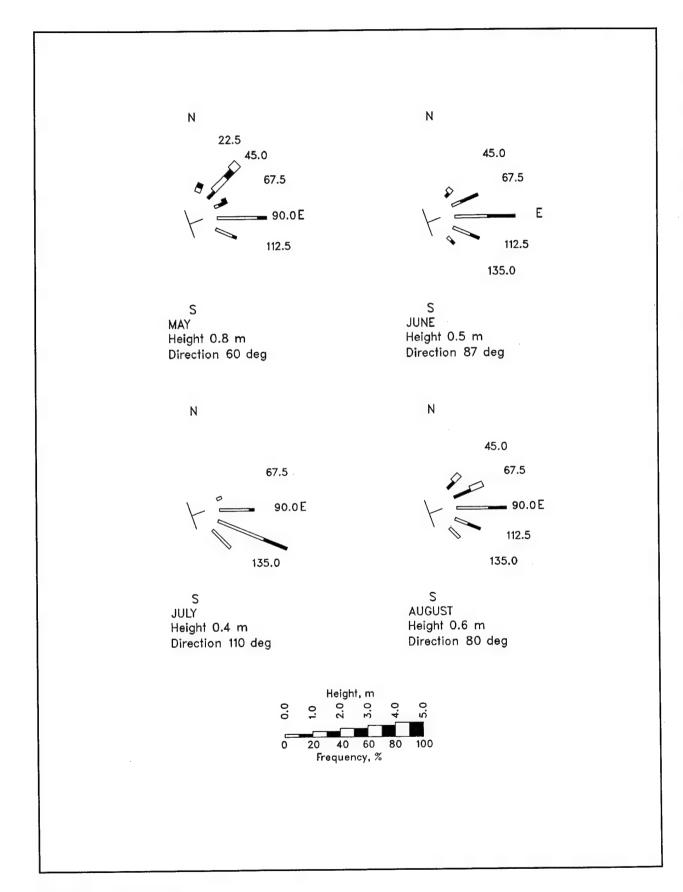


Figure 14. (Continued)

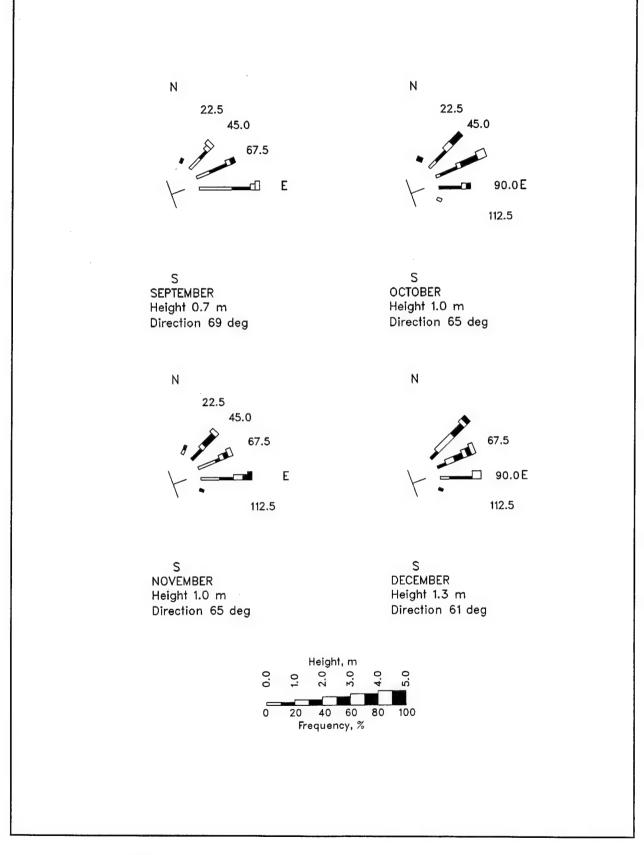


Figure 14. (Concluded)

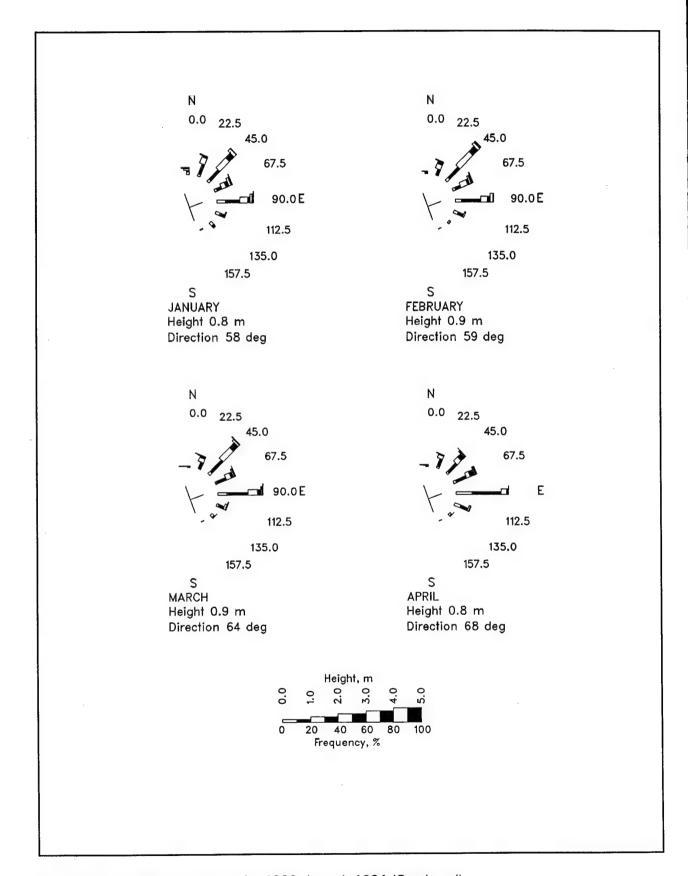


Figure 15. Monthly wave roses for 1980 through 1994 (Continued)

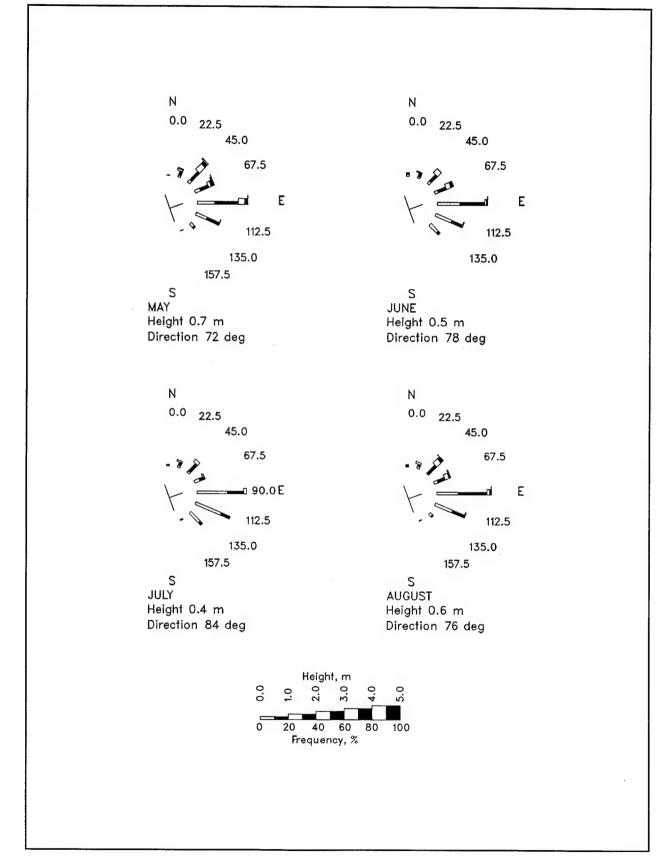


Figure 15. (Continued)

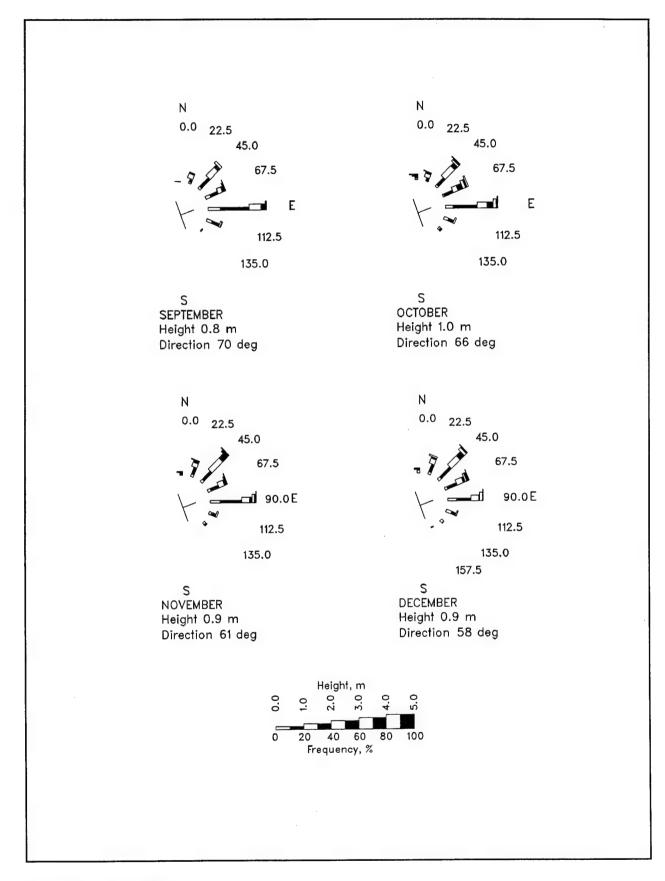


Figure 15. (Concluded)

4 Currents

Surface current speed and direction at the FRF are influenced by winds, waves, and, indirectly, by the bottom topography. The extent of the respective influences varies daily. However, winds tend to dominate the currents at the seaward end of the pier, whereas waves dominate within the surf zone.

Observations

Near 0700 EST, daily observations of surface current speed and direction were made at (a) the seaward end of the pier, (b) the midsurf position on the pier, and (c) 10 to 15 m from the beach 500 m updrift of the pier. Surface currents were determined by observing the movement of dye on the water surface.

Results

Annual mean and mean currents for 1980 through 1994 are presented in Table 6 and in Figure 16. Figure 16 shows the daily and average annual measurements at the beach, pier midsurf, and pier end locations. Since the relative influences of the winds and waves vary with position from shore, the current speeds and, to some extent, direction vary at the beach, midsurf, and pier end locations. Magnitudes generally are largest at the midsurf location and lowest at the end of the pier.

Table 6

Mean Longshore Surface Currents¹

	Pier End, cm/sec 1980-		<u>Pier Midsu</u>	rf, cm/sec 1980-	Beach, cm/sec 1980-		
<u>Month</u>	<u>1994</u>	1994	<u>1994</u>	1994	<u>1994</u>	1994	
Jan	17	21	18	17	11	9	
Feb	17	18	15	19	9	10	
Mar	8	12	4	5	2	6	
Apr	6	15	-5	3	4	2	
May	14	16	16	1	14	4	
Jun	-7	5	-19	-12	-5	-5	
Jul	5	4	-7	-8	-4	-7	
Aug	12	12	10	-2	5	-1	
Sep	17	11	16	5	11	3	
Oct	20	10	21	8	13	5	
Nov	15	9	21	7	6	3	
Dec	28	18	38	20	-5	4	
Annual	13	13	11	5	5	3	

^{1 + =} southward; - = northward.

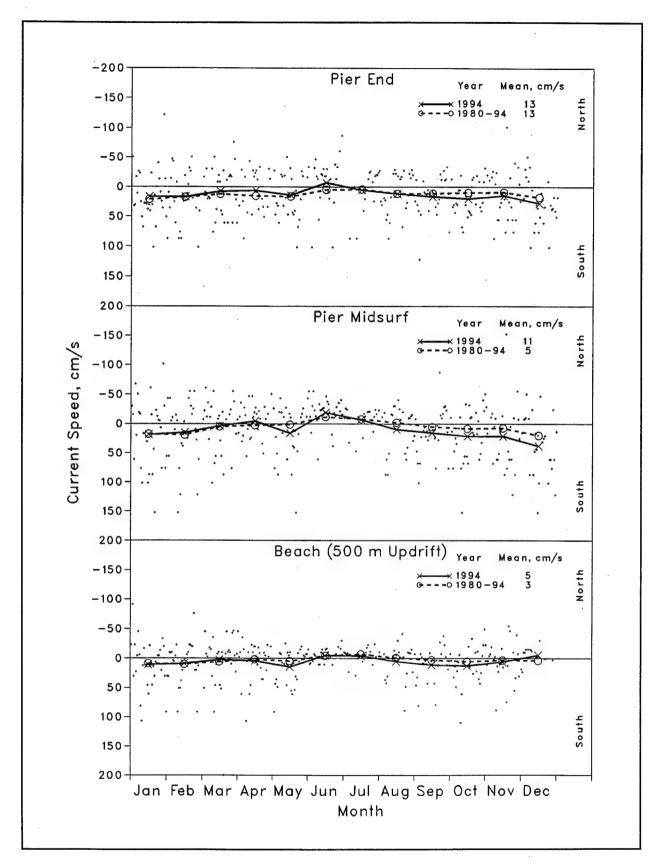


Figure 16. Daily current speeds and directions with monthly means for 1994

5 Tides and Water Levels

Measurement Instrument

Water level data were obtained from an NOAA/NOS control tide station (sta 865-1370) located at the seaward end of the research pier (Figure 2) by using a Leupold and Stevens, Inc. (Beaverton, OR), digital tide gauge. This analog-to-digital recorder is a float-activated, negator-spring, counterpoised instrument that mechanically converts the vertical motion of a float into a coded, punched paper tape record. The below-deck installation at pier sta 19+60 consisted of a 30.5-cm-diam stilling well with a 2.5-cm orifice and a 21.6-cm-diam float.

Operation and tending of the tide gauge conformed to NOS standards. The gauge was checked daily for proper operation of the punch mechanism and for accuracy of the time and water level information. The accuracy was determined by comparing the gauge level reading with a level read from a reference electric tape gauge. Once a week, a heavy metal rod was lowered down the stilling well and through the orifice to ensure free flow of water into the well. During the summer months, when biological growth was most severe, divers inspected and cleaned the orifice opening as required.

The tide station was inspected quarterly by an NOAA/NOS tide field group. Tide gauge elevation was checked using existing NOS control positions, and the equipment was checked and adjusted as needed. Both NOS and FRF personnel also reviewed procedures for tending the gauge and handling the data. Any specific comments on the previous months of data were discussed to ensure data accuracy.

Digital paper tape records of tide heights taken every 6 min were analyzed by the Tides Analysis Branch of NOS. An interpreter created a digital magnetic computer tape from the punch paper tape, which was then processed on a large computer. First, a listing of the instantaneous tidal height values was created for visual inspection. If errors were encountered, a computer program was used to fill in or recreate bad or missing data using correct values from the nearest NOS tide station and accounting for known time lags and elevation anomalies. The data were plotted, and a new listing was generated and rechecked. When the validity of the data had been confirmed, monthly tabulations of daily highs and lows, hourly heights (instantaneous

height selected on the hour), and various extreme and/or mean water level statistics were computed.

Results

Tides at the FRF are semidiurnal with both daily high and low tides approximately equal. Tide height statistics are presented in Table 7. Figure 17 plots the monthly tide statistics for all available data, and Figure 18 compares the distribution of daily high and low water levels and hourly tide heights. The monthly or annual mean sea level (MSL) reported is the average of the hourly heights, whereas the mean tide level is midway between mean high water (MHW) and mean low water (MLW), which are the averages of the daily high- and low-water levels, respectively, relative to NGVD. Mean range (MR) is the difference between MHW and MLW levels, and the lowest water level for the month is the extreme low (EL) water, while the highest water level is the extreme high (EH) water level.

NOTE: Due to a mistake in converting feet to centimeters the tide height statistics from 1987 through 1993 (As published in the 1987 through 1993 Annual Data Summaries) found in Table 7 and Figure 17 were in error. These have been corrected for this report.

Table 7
Tide Height Statistics¹

Month or <u>Year</u>	Mean High <u>Water</u>	Mean Tide <u>Level</u>	Mean Sea <u>Level</u>	Mean Low <u>Water</u>	Mean Range	Extreme High	<u>Date</u>	Extreme Low	<u>Date</u>
					<u>1994</u>				
Jan	51	0	0	-52	103	106	27	-95	11
Feb	59	9	9	-41	100	111	24	-78	26
Mar	64	12	12	-41	105	107	4	-78	28
Apr	51	0	1	-51	102	107	27	-81	25
May	70	20	21	-30	100	116	24	-55	26
Jun	56	6	7	-44	100	98	22	-73	27
Jul	52	4	5	-45	97	80	19	-80	23
Aug	59	10	11	-38	97	96	6	-68	15
Sep	71	22	23	-27	98	119	4	-56	7
Oct	76	26	27	-23	99	106	3	-53	7
Nov	63	12	12	-39	102	122	18	-92	4
Dec	70	19	20	-32	102	103	15	-87	3
1994	62	12	12	-39	101	122	Nov	-95	Jan
				Ē	Prior Year	<u>'s</u>			
1993	67	18	19	-31	98	150	Dec	-84	Nov
1992	66	17	17	-32	98	150	Dec	-84	Nov
1991	66	18	18	-31	97	150	Oct	-100	Dec
1990	59	11	11	-38	97	131	May	-94	Feb
1989	59	11	11	-37	96	239	Mar	-92	Apr
1988	55	7	7	-40	95	155	Apr	-86	Dec
1987	66	18	19	-29	95	136	Jan	-76	Nov
1986	60	13	13	-35	95	123	Dec	-108	Jan
1985	59	10	11	-37	96	136	Dec	-93	Apr
1984	64	16	.16	-32	97	147	Oct	-77	Jul
1983	68	19	19	-30	98	143	Jan	-73	Mar
1982	58	8	. 9	-42	99	127	Oct	-108	Feb
1981	59	8	9	-42	101	149	Nov	-110	Apr
1980	59	8	8	-43	102	118	Mar	-119	Mar
1979	60	9	9	-43	103	121	Feb	-95	Sep
1979-									

¹ Measurements are in centimeters.

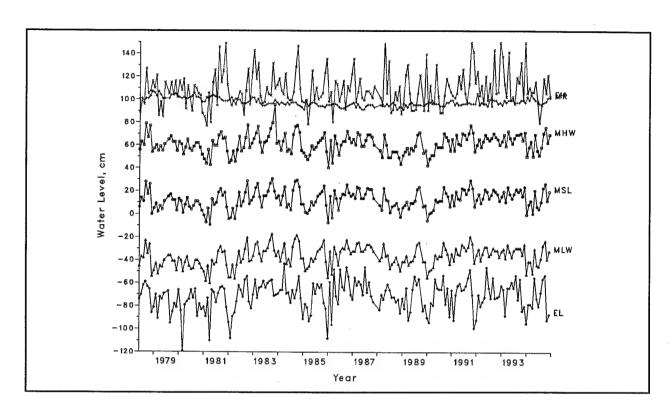


Figure 17. Monthly tide and water level statistics relative to NGVD

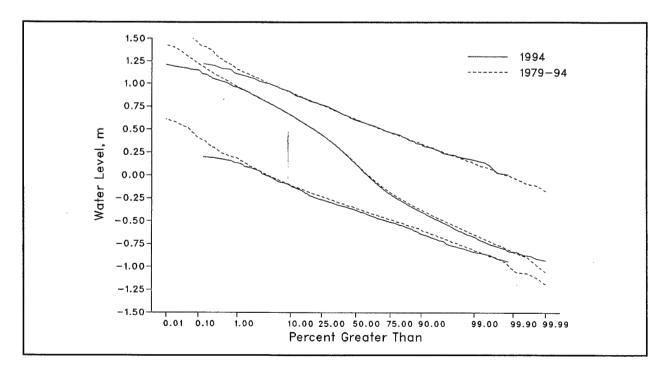


Figure 18. Distributions of hourly tide heights and high- and low-water levels

6 Water Characteristics

Monthly averages of daily measurements of surface water temperature, visibility, and density at the seaward end of the FRF pier are given in Table 8. The summaries represent single observations made near 0700 EST and, therefore, may not reflect daily average conditions since such characteristics can change within a 24-hr period. Large temperature variations were common when there were large differences between the air and water temperatures and variations in wind direction. From past experience, persistent onshore winds move warmer surface water toward the shoreline, although offshore winds cause colder bottom water to circulate shoreward, resulting in lower temperatures.

Burface Water (Charas	toriotico				
irtace water	Cnarac	tensucs				
	Temper	ature	Visib	oility	Dens	ity
		1 C	п	•	g/c	
		1980-		1980-		1980-
<u>Month</u>	1994	1994	<u>1994</u>	1994	1994	1994
Jan	5.3	6.3	1.4	1.3	1.0239	1.0233
Feb	4.4	5.6	1.9	1.8	1.0215	1.0230
Mar	6.7	7.1	1.5	1.5	1.0218	1.0227
Apr	11.3	11.0	1.8	1.9	1.0213	1.0222
May	15.7	15.3	1.8	2.3	1.0205	1.0217
Jun	21.0	19.5	3.3	3.3	1.0207	1.0212
Jul	21.6	21.8	3.1	3.7	1.0232	1.0215
Aug	21.1	23.4	2.9	3.2	1.0222	1.0206
Sep	22.2	23.0	2.3	2.2	1.0216	1.0209
Oct	18.1	19.3	1.1	1.5	1.0219	1.0218
Nov	15.7	14.9	0.8	1.1	1.0236	1.0229
Dec	11.2	10.1	0.6	1.1	1.0229	1.0234
Annual	14.5	14.8	1.9	2.1	1.0221	1.0221

Temperature

Daily sea surface water temperatures (Figure 19) were measured with an NOS water sampler and thermometer. Monthly mean water temperatures (Table 8) varied with the air temperatures (see Table 2).

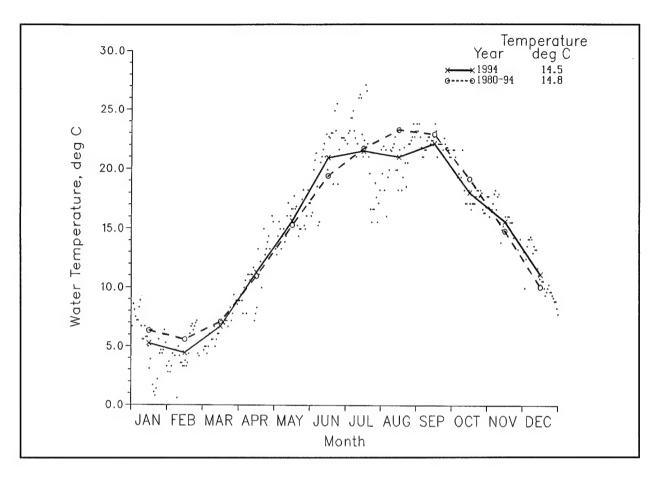


Figure 19. Daily water temperature values with monthly means

Visibility

Visibility in coastal nearshore waters depends on the amount of salts, soluble organic material, detritus, living organisms, and inorganic particles in the water. These dissolved and suspended materials change the absorption and attenuation characteristics of the water that vary daily and yearly.

Visibility was measured with a 0.3-m-diam Secchi disk, and similar to water temperature, variation was related to onshore and offshore winds. Onshore winds moved warm clear surface water toward shore, whereas offshore winds brought up colder bottom water with large concentrations of suspended matter. Figure 20 presents the daily and monthly mean surface visibility values for the year. Large variations were common, and visibility less than 1 m was expected in any month. Monthly means are given in Table 8.

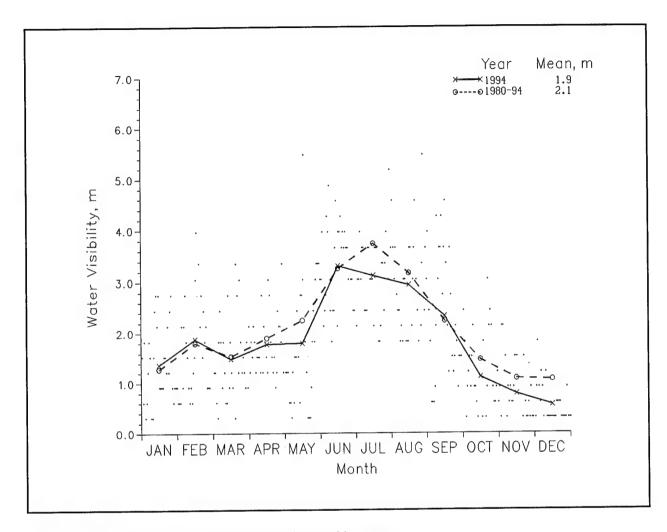


Figure 20. Daily water visibility values with monthly means

Density

Daily and monthly mean surface density values, plotted in Figure 21, were measured with a hydrometer. Monthly means are also given in Table 8. These values are direct readings from the hydrometer. Corrections for differences between ocean water temperature and jar water temperature, as well as use of uncalibrated hydrometers and other factors, could produce an error amounting to a couple of percent in the direct hydrometer readings.

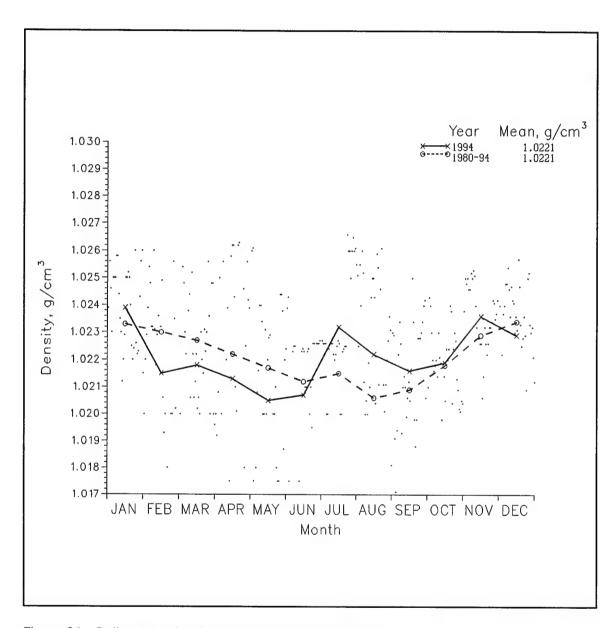


Figure 21. Daily water density values with monthly means

7 Surveys

Waves and currents interacting with bottom sediments produce changes in the beach and nearshore bathymetry. These changes can occur very rapidly in response to storms, or slowly as a result of persistent but less forceful seasonal variations in wave and current conditions.

Nearshore bathymetry at the FRF is characterized by regular shore-parallel contours, a moderate slope, and a barred surf zone (usually an outer storm bar in water depths of about 4.5 m and an inner bar in water depths between 1.0 and 2.0 m). This pattern is interrupted in the immediate vicinity of the pier where a permanent trough runs under much of the pier, ending in a scour hole where depths can be up to 3.0 m greater than the adjacent bottom (Figure 22). This trough, which apparently is the result of the interaction of waves and currents with the pilings, varies in shape and depth with changing wave and current conditions. The effect of the pier on shore-parallel contours occurs as far as 300 m away, and the shoreline may be affected up to 350 m from the pier (Miller, Birkemeier, and DeWall 1983).

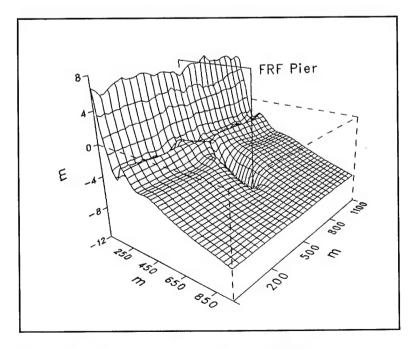


Figure 22. Permanent trough under the FRF pier, 24 January 1994

Approximately once a month, surveys were conducted of an area extending 600 m north and south of the pier and approximately 950 m offshore. These surveys were conducted to document the temporal and spatial variability in bathymetry. Contour maps resulting from these surveys, along with plots of change in elevation between surveys, are given in Appendix A.

All surveys used the Coastal Research Amphibious Buggy (CRAB), a 10.7-m-tall amphibious tripod described by Birkemeier and Mason (1984), in combination with a Geodimeter 140-T self-tracking, electronic theodolite, distance meter. Profile locations are shown in each figure in Appendix A. Monthly soundings along both sides of the FRF pier were collected by lowering a weighted measuring tape to the bottom and recording the distance below the pier deck. Soundings were taken midway between the pier pilings to minimize errors caused by scour near the pilings.

A history of bottom elevations below Gauges 645 and 625 is presented in Figure 23 for pier stations 7+80 (238 m) and 18+60 (567 m), along with intermediate locations, 323 and 433 m.

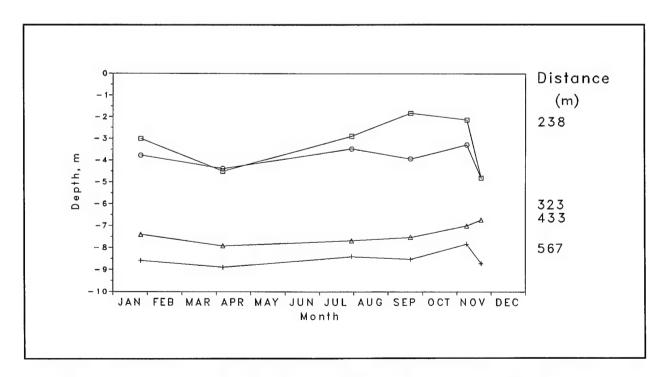


Figure 23. Time-history of bottom elevations at selected locations under the FRF pier

8 Photography

Aerial Photographs

Aerial photographs were taken biannually using a 23-cm aerial mapping camera at a scale of 1:12,000. All coverage was at least 60-percent overlap, with flights flown as closely as possible to low tide between 1000 and 1400 EST with less than 10-percent cloud cover. The flight lines covered are shown in Figure 24. Figure 25 is a sample of the imagery obtained on 14 January 1991; the available aerial photographs for the year are:

<u>Date</u>	Flight Lines	<u>Format</u>
22 January	1 2	Black/White Color

Beach Photographs

Daily color slides of the beach were taken using a 35-mm camera from the same location on the pier looking north and south (Figure 26). The location from which each picture was taken, as well as the date, time, and a brief description of the picture, were marked on each of the slides.

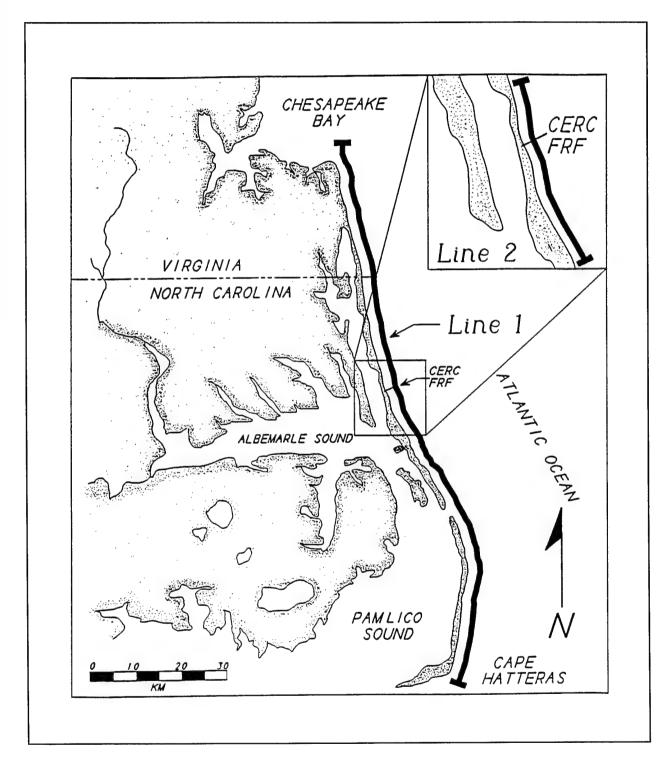


Figure 24. Aerial photography flight lines

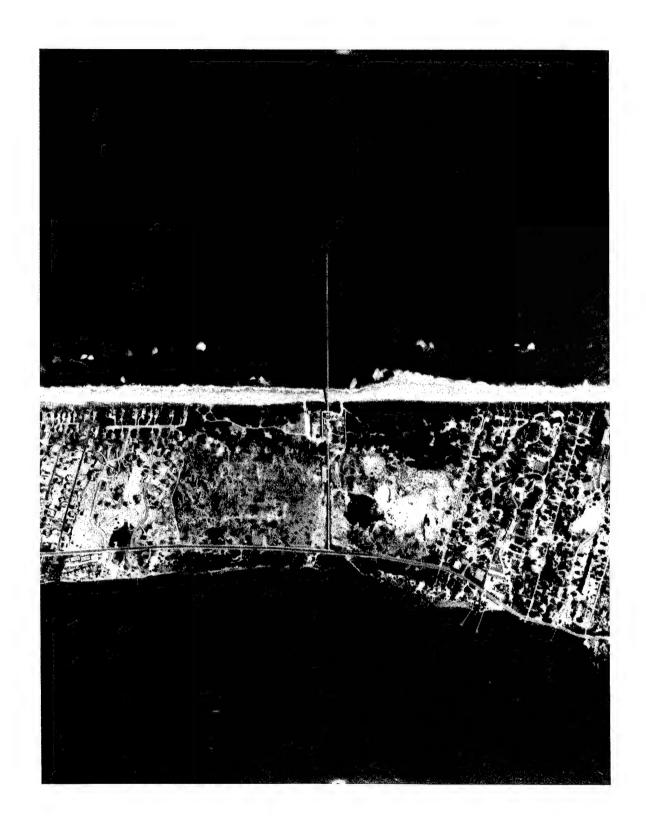


Figure 25. Sample aerial photograph, 14 January 1991 (Scale = 1:12,000)

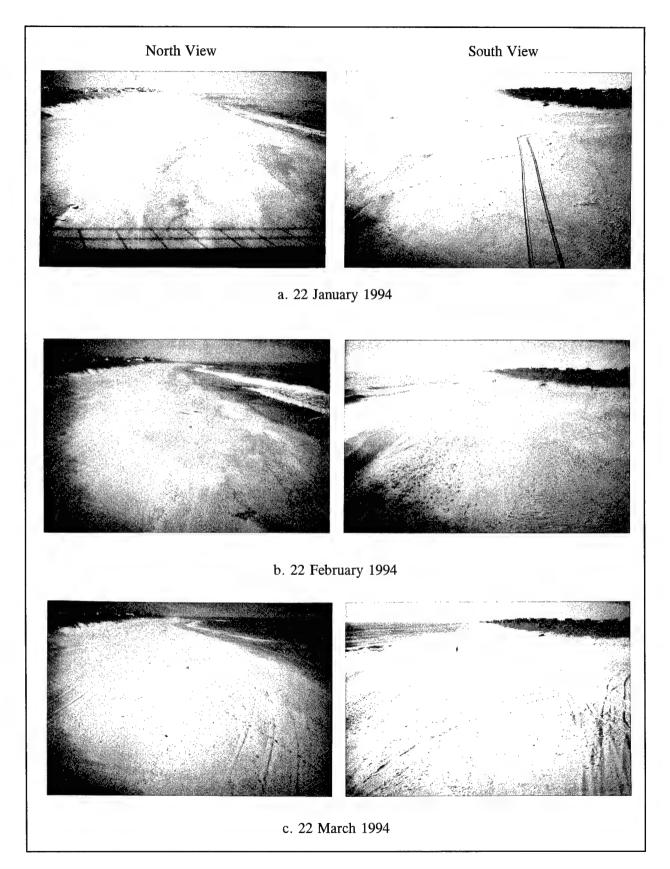


Figure 26. Beach photos looking north and south from the FRF pier (Sheet 1 of 4)

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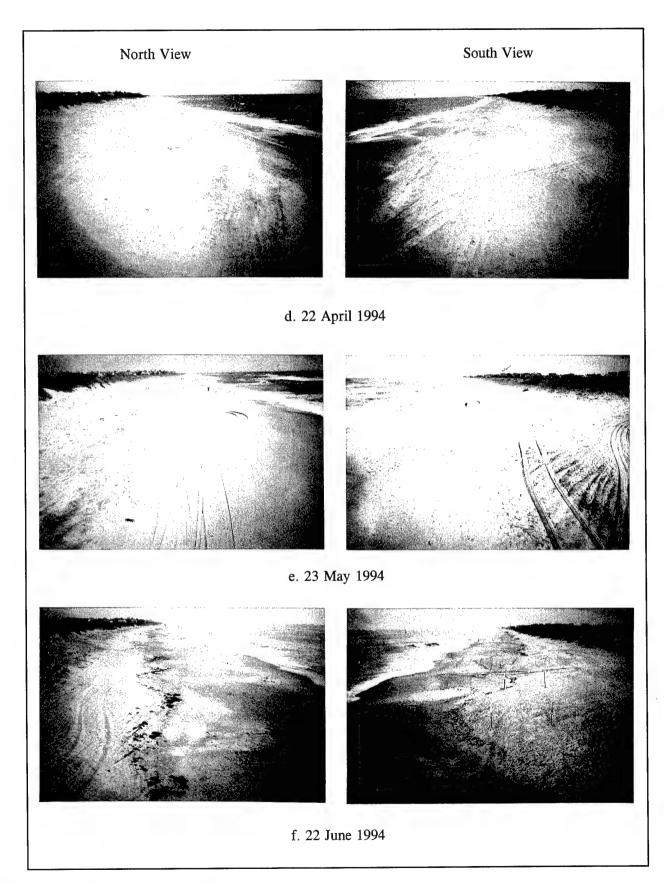


Figure 26. (Sheet 2 of 4)

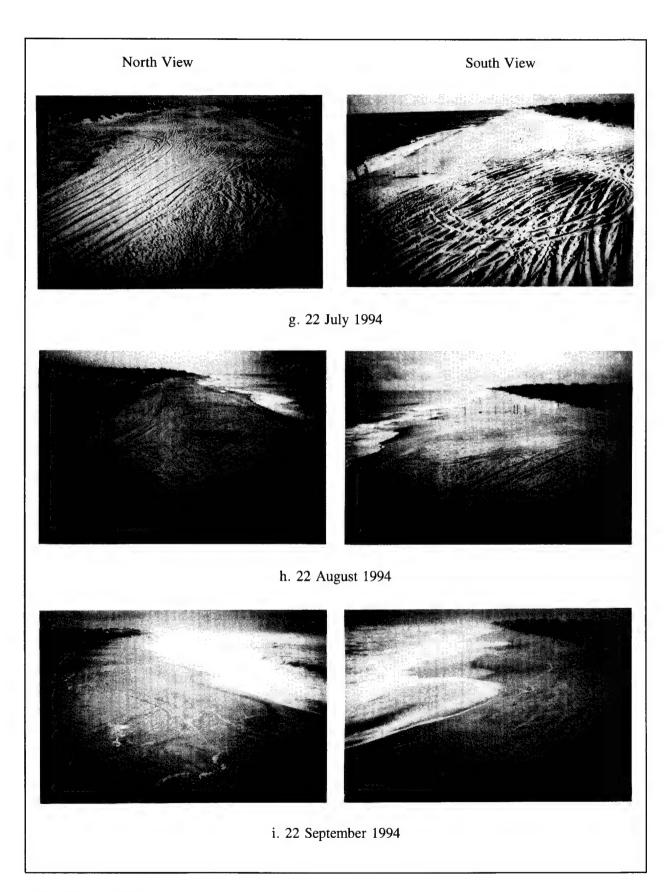


Figure 26. (Sheet 3 of 4)

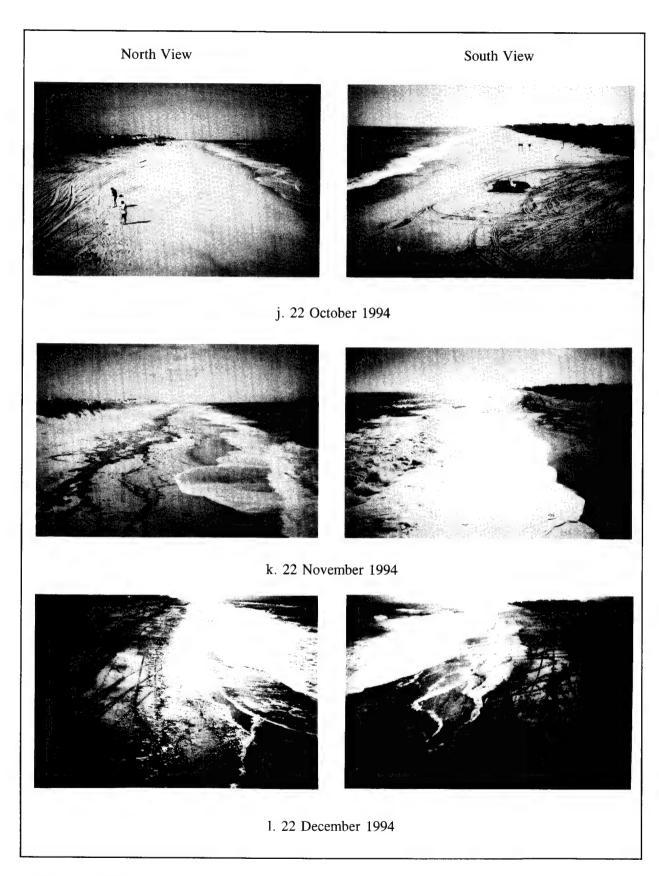


Figure 26. (Sheet 4 of 4)

9 Storms

This chapter discusses storms (defined here as times when the wave height parameter H_{mo} equaled or exceeded 2 m at the seaward end of the FRF pier). Sample spectra from Gauge 630 are given in Appendix B. Prestorm and/or poststorm bathymetry diagrams are given in Appendix A. Tracking information was provided by NOAA Daily Weather Maps (U.S. Department of Commerce 1994).

3-4 January 1994 (Figure 27)

Forming off the Georgia/South Carolina border this storm quickly moved up the North Carolina coast. Maximum onshore winds (from northeast) reached 13 m/sec at 2042 EST on 3 January. The minimum atmospheric pressure was 991 mb while the maximum H_{mo} (at Gauge 630) was 3.14 m ($T_p=7.76~{\rm sec}$) at 1934 EST also on 3 January. There was 48 mm of precipitation.

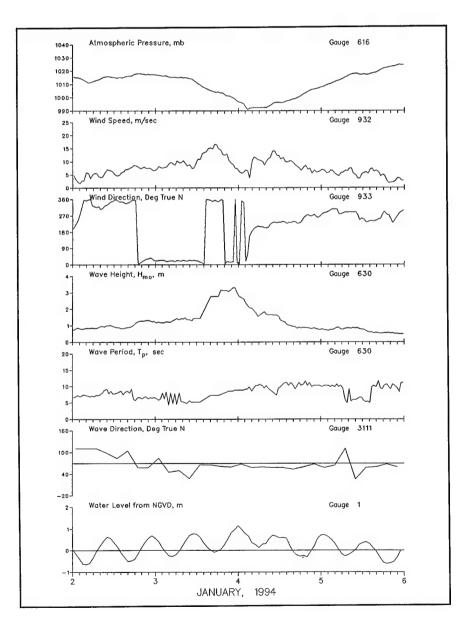


Figure 27. Data for 3-4 January 1994 storm

26-28 January 1994 (Figure 28)

A strong Canadian high pressure system produced maximum onshore winds (from northeast) of 11 m/sec at 0508 EST on 27 January. Waves at Gauge 630 reached a maximum H_{mo} of 2.97 m ($T_p=12.19~{\rm sec}$) at 0916 EST on 27 January. There was 12 mm of precipitation.

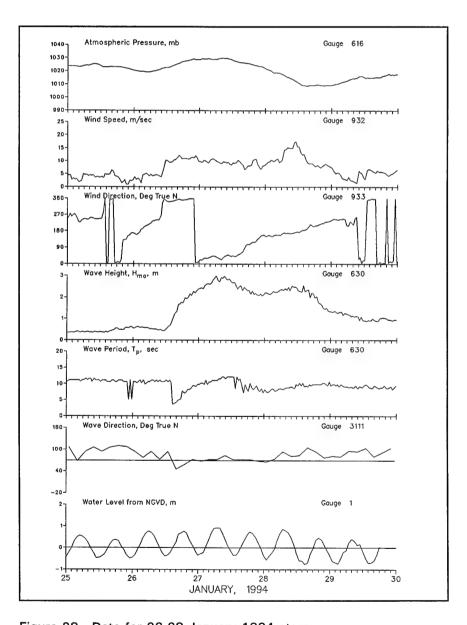


Figure 28. Data for 26-28 January 1994 storm

30-31 January 1994 (Figure 29)

Northeasterly winds funneled between a Canadian high pressure system and a small low pressure system located offshore of Cape Hatteras, NC, generated storm waves at the FRF. Waves at Gauge 630 reached a maximum H_{mo} of 2.78 m ($T_p=7.53~{\rm sec}$) at 2200 EST on 30 January. Onshore winds (from northeast) peaked at 13.4 m/sec at 1516 EST on 30 January. The FRF received 20 mm of precipitation from this storm.

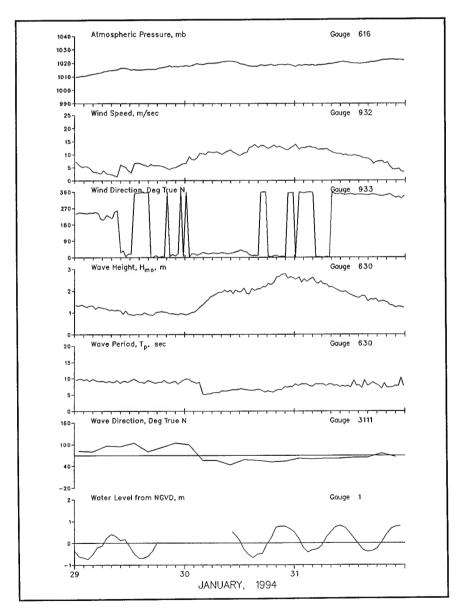


Figure 29. Data for 30-31 January 1994 storm

2-3 March 1994 (Figure 30)

Forming over Georgia early on 2 March this storm quickly moved up the eastern coast. Southeasterly winds approaching 17 m/sec peaked at 1300 EST on 2 March, followed by the maximum H_{mo} (at Gauge 630) of 3.4 m ($T_p = 11.6~{\rm sec}$) which was recorded later that afternoon at 2116 EST. The minimum atmospheric pressure at the FRF was 989 mb. There was 77 mm of precipitation.

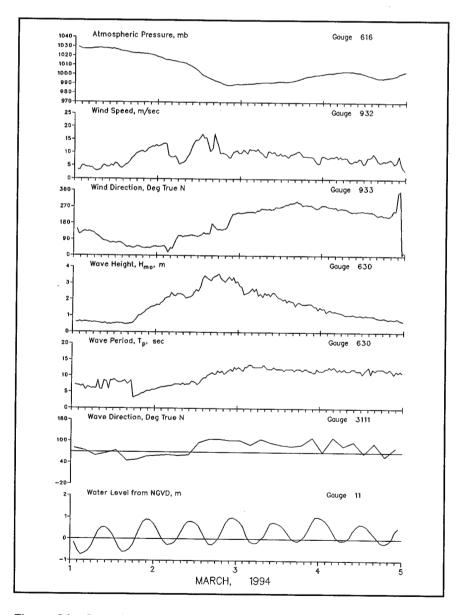


Figure 30. Data for 2-3 March 1994 storm

4 May 1994 (Figure 31)

Forming off the North Carolina coast early on 4 May and then rapidly moving offshore, this intense storm produced maximum onshore winds (from northeast) at the FRF approaching 19 m/sec at 1000 EST on 4 May. The maximum H_{mo} (at Gauge 630) of 4.11 m ($T_p = 9.1$ sec) was measured soon after at 1034 EST. The minimum atmospheric pressure recorded at the FRF was 1006 mb. There was 84 mm of precipitation.

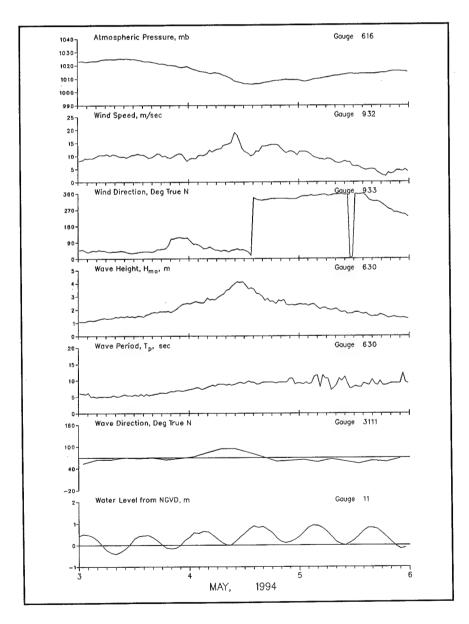


Figure 31. Data for 4 May 1994 storm

20-21 May 1994 (Figure 32)

Strong winds associated with a high pressure system reached 15 m/sec (from northeast) at 0808 EST on 21 May. The maximum H_{mo} (at Gauge 625) reached 2.19 m ($T_p=6.00~{\rm sec}$) at 1000 EST on 21 May.

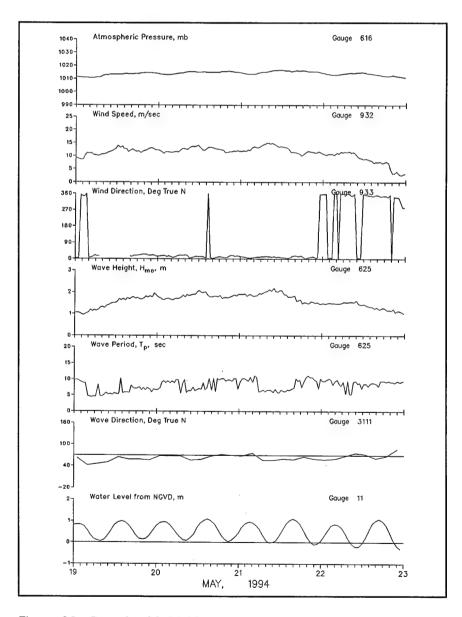


Figure 32. Data for 20-21 May 1994 storm

3-5 September 1994 (Figure 33)

A combination of a Canadian high pressure system and a low off the North Carolina coast produced onshore winds (from northeast) of 16 m/sec at 1000 EST on 4 September. The maximum H_{mo} (at Gauge 630) reached 2.9 m ($T_p=8.0~{\rm sec}$) at 1300 EST also on 4 September. There was 10 mm of precipitation.

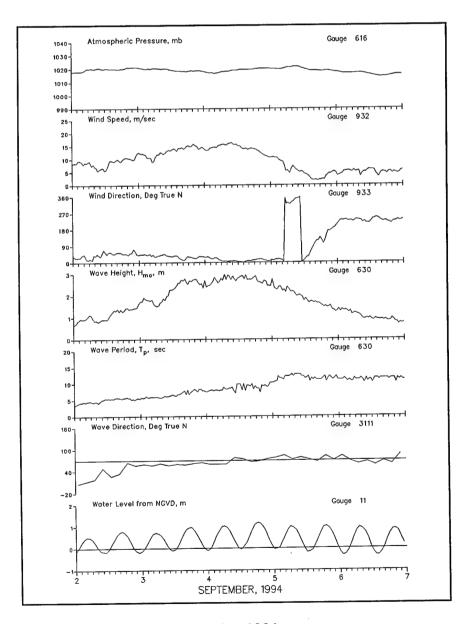


Figure 33. Data for 3-5 September 1994 storm

22 September 1994 (Figure 34)

Northeasterly winds associated with a western high pressure system and a low pressure system northeast of the FRF reached 17 m/sec at 0316 EST on 22 September. Also measured at the same time was the maximum H_{mo} (at Gauge 625) of 2.4 m ($T_p=8.26~{\rm sec}$). There was 64 mm of precipitation.

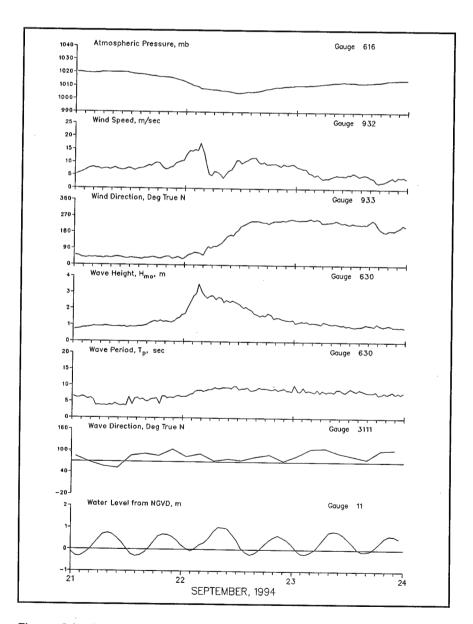


Figure 34. Data for 22 September 1994 storm

3 October 1994 (Figure 35)

A combination of a Canadian high pressure system and a storm located southest of Cape Hatteras, NC generated strong onshore winds. The maximum H_{mo} (at Gauge 625) of 2.3 m ($T_p=6.7~{\rm sec}$) was attained at 1334 EST on 3 October. Maximum winds (from northeast) reached 15 m/sec several hours earlier at 1100 EST. There was no precipitaion.

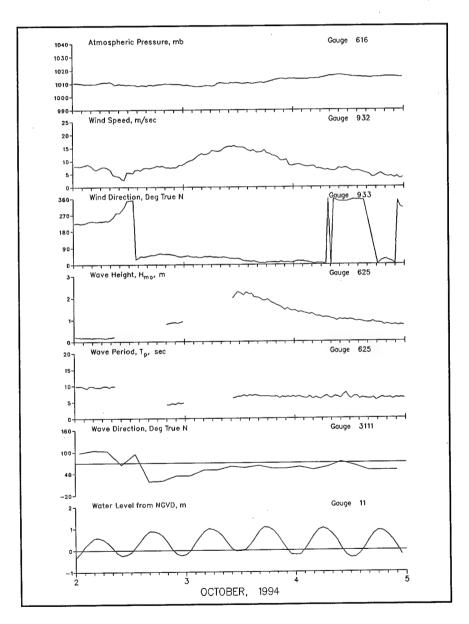


Figure 35. Data for 3 October 1994 storm

12-13 October 1994 (Figure 36)

Northeasterly winds associated with a high pressure system over New England and and a developing low in the Gulf of Mexico began to increase at the FRF on 11 October. Crossing Florida, the storm continued to intensify as it stalled south of Cape Hatteras, NC. Blocked by a northern high pressure system the storm slowly weakened. Maximum onshore winds (from northeast) reached 15 m/sec at 2116 EST on 12 October. The maximum H_{mo} (at Gauge 625) was 2.3 m ($T_p = 6.9~{\rm sec}$) at 1742 also on 12 October. There was no precipitation.

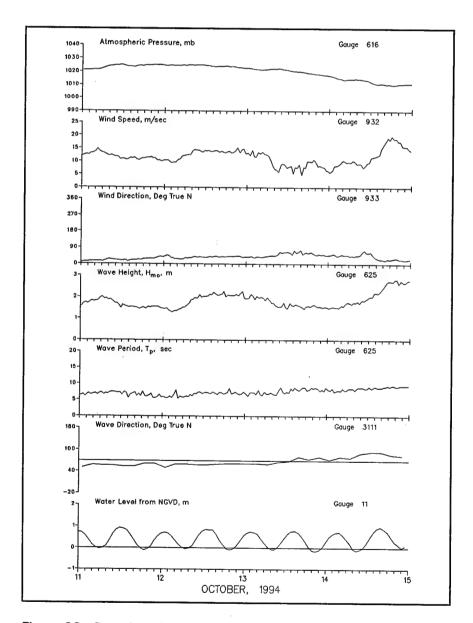


Figure 36. Data for 12-13 October 1994 storm

14-17 October 1994 (Figure 37)

The weak storm located southeast of Cape Hatteras, NC, on 13 October reintensified as it approached the North Carolina coast. Maximum onshore winds (from northeast) reached 20 m/sec at 1816 EST on 14 October. The maximum H_{mo} (at Gauge 630) reached 4.5 m ($T_p=11.1~{\rm sec}$) at 1300 EST on 15 October. There was 92 mm of precipitation.

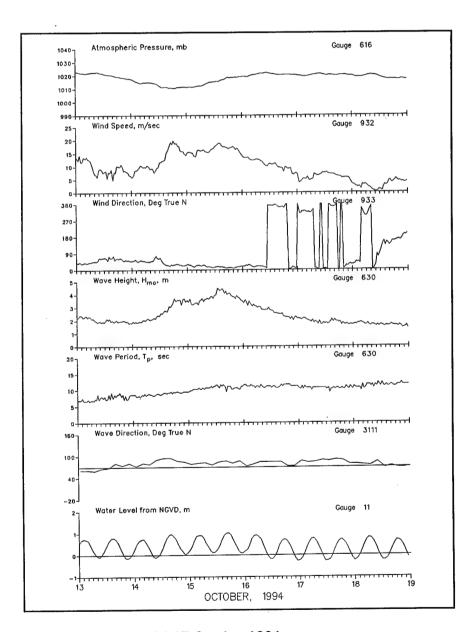


Figure 37. Data for 14-17 October 1994 storm

7 November 1994 (Figure 38)

Northeasterly winds produced by a Canadian high pressure system generated storm waves at the FRF. The maximum H_{mo} (at Gauge 625) was 2.00 m ($T_p=7.1~{\rm sec}$) at 0916 EST on 7 November. Onshore winds reached 17 m/sec at 0616 EST. There was no precipitation.

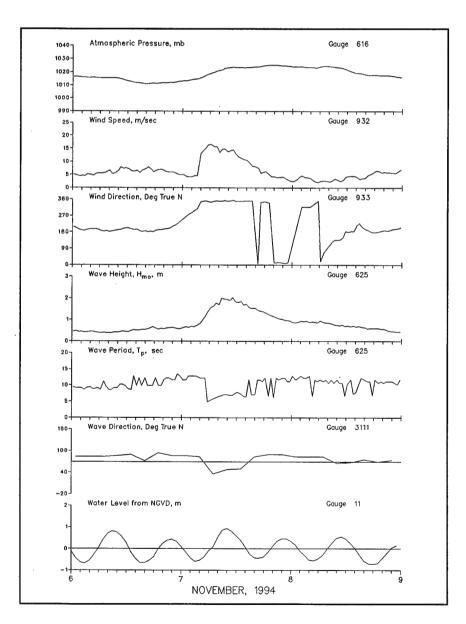


Figure 38. Data for 7 November 1994 storm

10 November 1994 (Figure 39)

Following the passage of a cold front strong northeasterly winds (16 m/sec) generated a maximum H_{mo} (at Gauge 625) of 2.3 m ($T_p = 7.5$ sec) at 1334 EST on 10 November. There was 41 mm of precipitation.

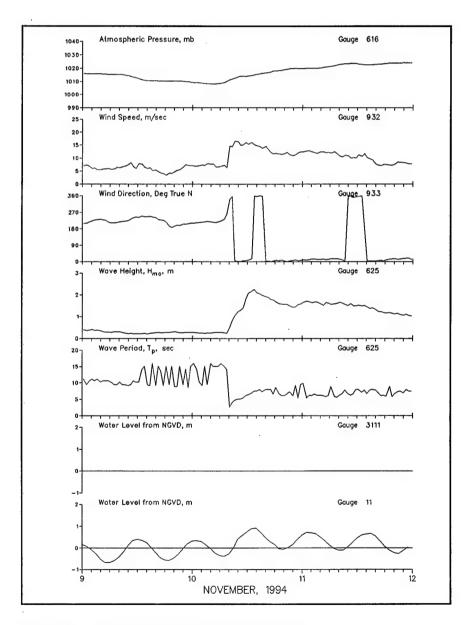


Figure 39. Data for 10 November 1994 storm

16-19 November 1994 (Figure 40)

While still located over southern Florida, Tropical Storm "Gordon's" interaction with a strong Canadian high pressure system produced northeasterly winds of 15 m/sec at 1816 EST on 16 November. Crossing Florida into the Atlantic, "Gordon" was located approximately 560 km south of Cape Hatteras, NC, on the morning of 17 November. Continuing to intensify, "Gordon" had, by early 18 November, been upgraded to a hurricane, before turning south to rapidly weaken and finally dissipate. The maximum H_{mo} (at Gauge 630) reached 5.0 m ($T_p = 12.8~{\rm sec}$) at 2342 EST on 17 November before the gauge broke free from its mooring. Minimum atmospheric pressure at the FRF was 1005 mb. There was 192 mm precipitation.

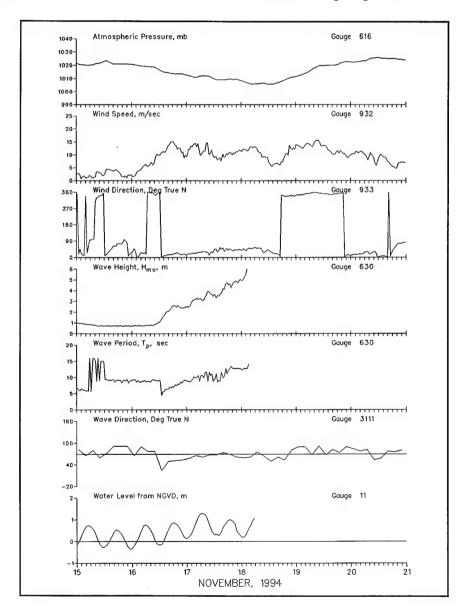


Figure 40. Data for 16-19 November 1994 Hurricane "Gordon"

8 December 1994 (Figure 41)

A Canadian high pressure system produced onshore winds (from the northeast) which peaked at 0700 EST on 8 December at 18 m/sec. The maximum H_{mo} (at Gauge 625) was 2.2 m ($T_p=6.9~{\rm sec}$) at 0808 EST. There was no precipitation.

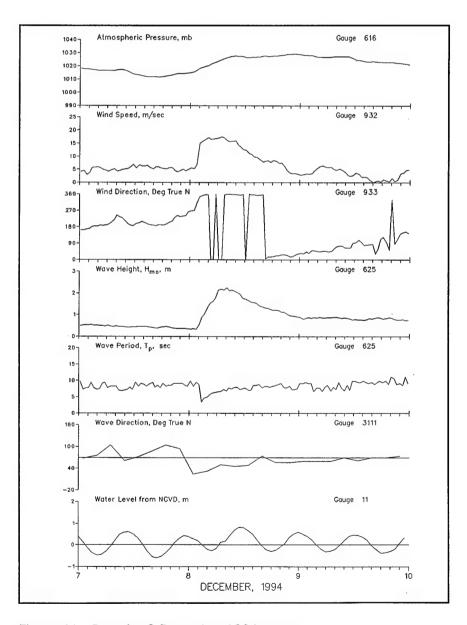


Figure 41. Data for 8 December 1994 storm

14-19 December 1994 (Figure 42)

A Canadian high pressure system produced onshore winds (from the northeast) which peaked at 1742 EST on 14 December at 17 m/sec. The development of a low pressure system off Cape Hatteras, NC, early on 18 December sustained the winds for another day. The maximum H_{mo} (at Gauge 630) was 3.8 m ($T_p = 9.1$ sec) at 2116 EST on 14 December. There was 34 mm of precipitation.

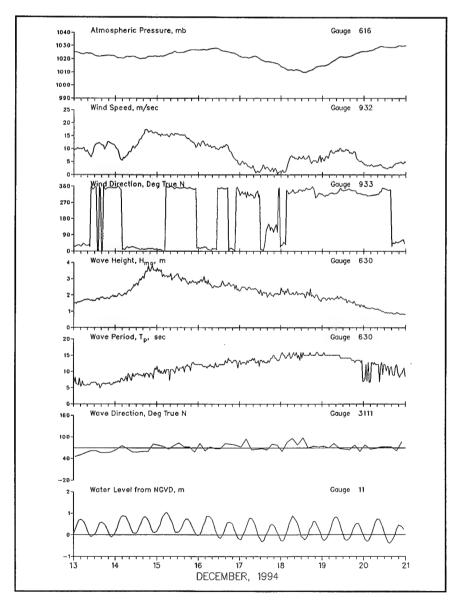


Figure 42. Data for 14-19 December 1994 storm

22-24 December 1994 (Figure 43)

Developing as the dominant storm from a pair of low pressure systems well off the North Carolina coast, this storm rapidly intensified as it passed Cape Hatteras, NC. The maximum H_{mo} (at Gauge 630) was 4.6 m ($T_p = 12.8~{\rm sec}$) at 2308 EST on 23 December. Maximum onshore winds (from northeast) reached 21 m/sec at 2308 EST also on 23 December. The minimum atmospheric pressure at the FRF was 995 mb. There was 17 mm of precipitation.

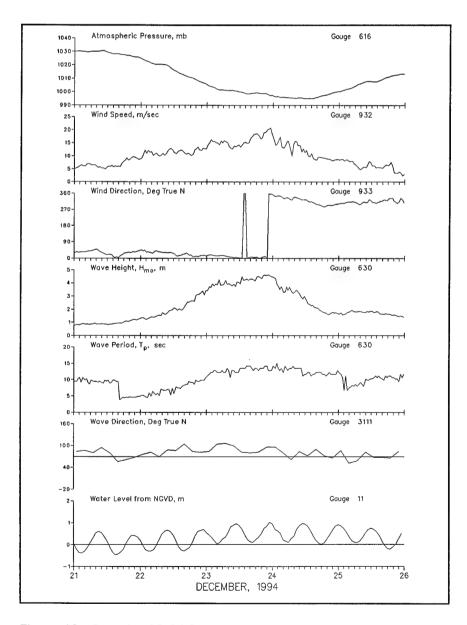


Figure 43. Data for 22-24 December 1994 storm

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Appendix A Survey Data

Contour diagrams constructed from the bathymetric survey data are presented in this appendix. The profile lines surveyed are identified on each diagram. Contours are in half-meter increments referenced to the National Geodetic Vertical Datum (NGVD). The distance offshore is referenced to the Field Research Facility (FRF) monumentation baseline behind the dune.

Changes in FRF bathymetry diagrams constructed by contouring the difference between two contour diagrams are also presented with contour intervals of 0.25 m. Wide contour lines show areas of erosion. Other areas correspond to areas of accretion. Although these change diagrams are based on considerable interpolation of the original survey data, they do facilitate comparison of the contour diagrams.

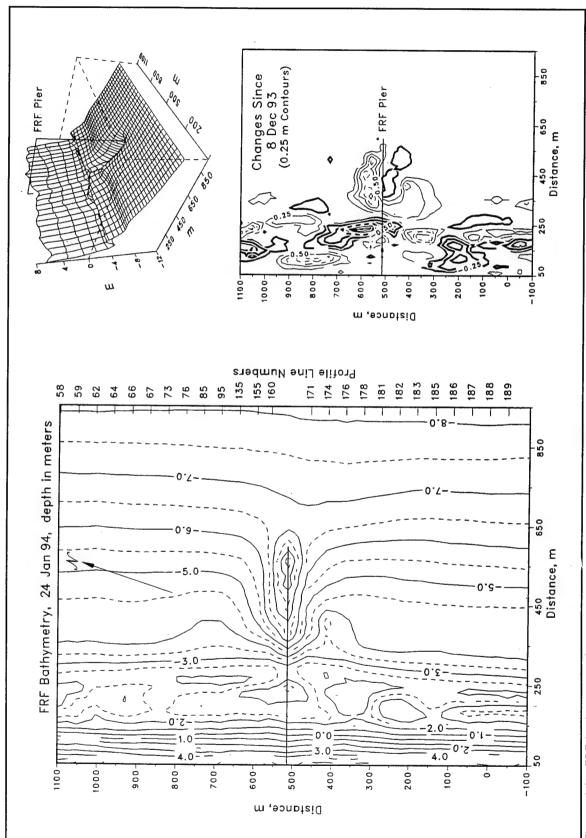


Figure A1. FRF bathymetry, 24 January 94 (depths relative to NGVD)

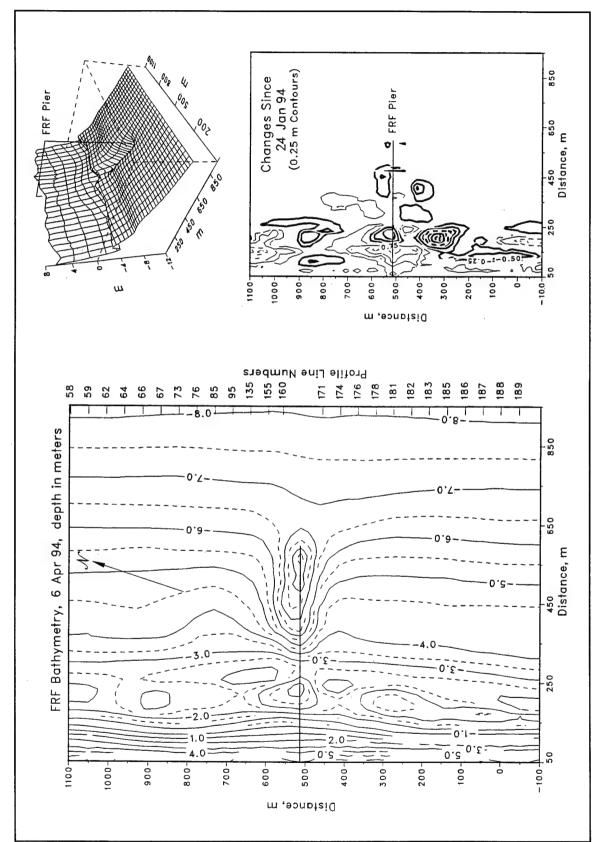
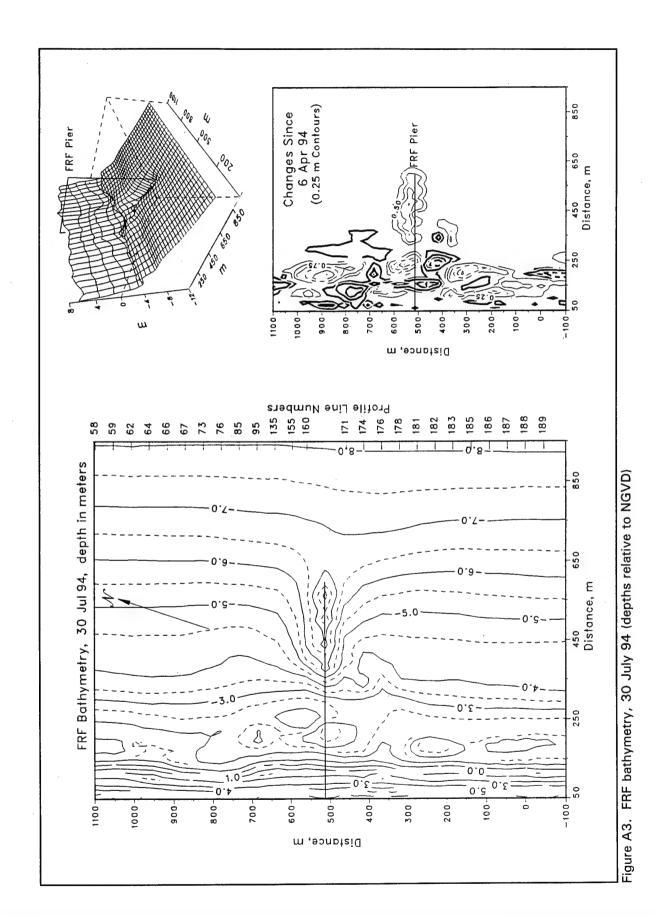
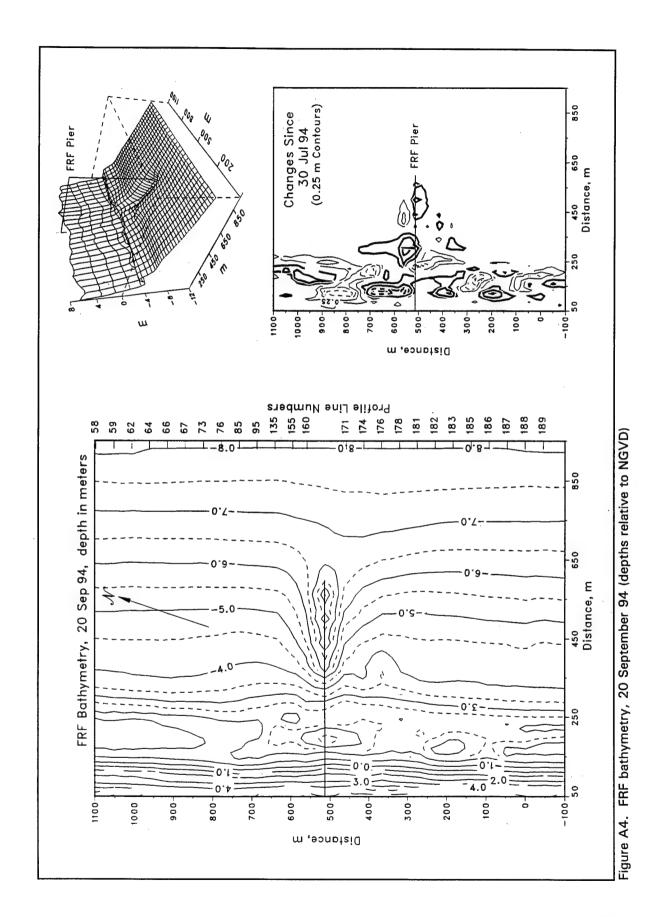


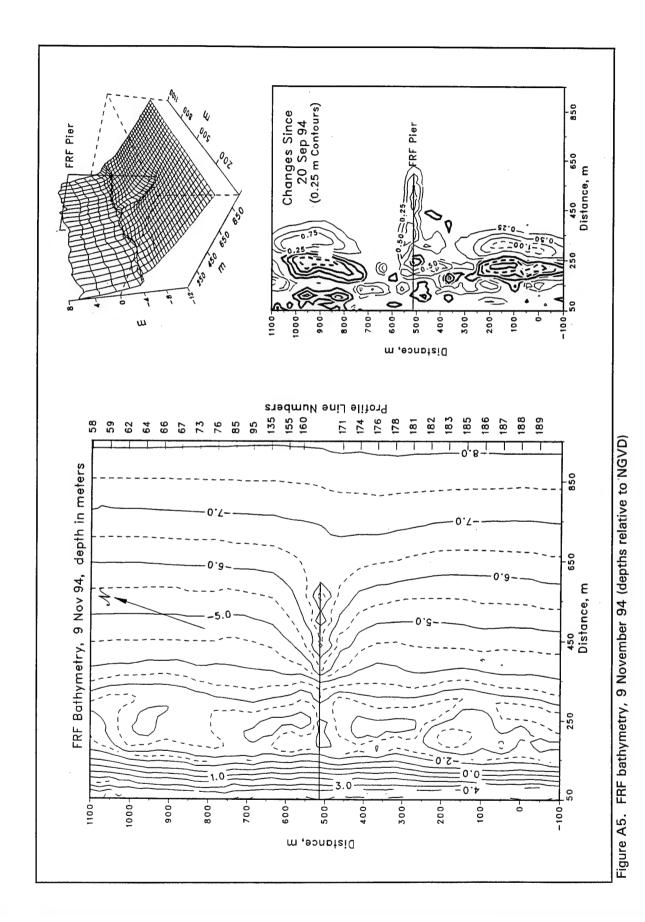
Figure A2. FRF bathymetry, 6 April 94 (depths relative to NGVD)



Α4



Α5



Α6

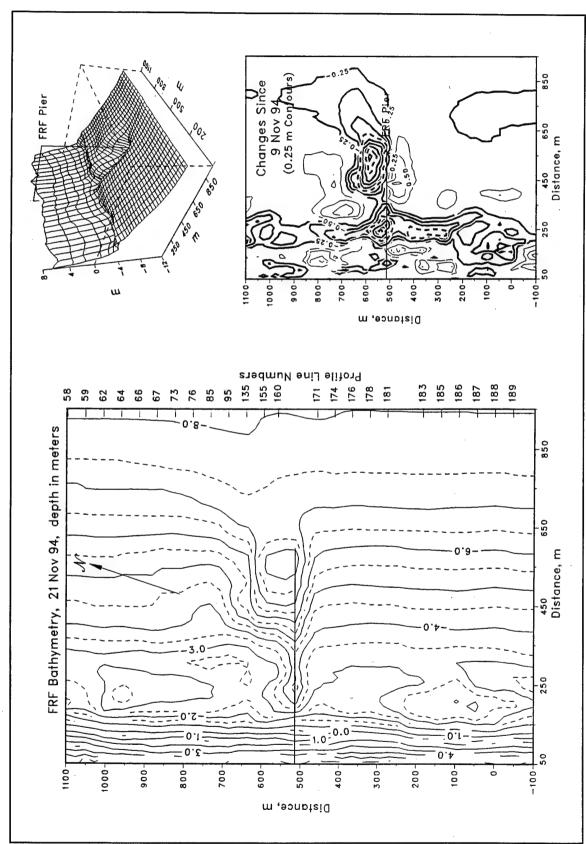


Figure A6. FRF bathymetry, 21 November 94 (depths relative to NGVD)

Appendix B Wave Data for Gauge 630

Wave data summaries for Gauge 630 for 1994 and for 1980 through 1994 are presented in the following pages.

Daily H_{mo} and T_p

Figure B1 displays the individual wave height H_{mo} and peak spectral wave period T_p values, along with the monthly mean values.

Joint Distributions of H_{mo} and T_{p}

Annual and monthly joint distribution tables are presented in Tables B1 and B2, and data for 1980 through 1994 are in Tables B3 and B4. Each table gives the frequency (in parts per 10,000) for which the wave height and peak period were within the specified intervals; these values can be converted to percentages by dividing by 100. Marginal totals are also included. The row total gives the number of observations out of 10,000 that fell within each specified peak period interval. The column total gives the number of observations out of 10,000 that fell within each specified wave height interval.

Cumulative Distributions of Wave Height

Annual and monthly wave height distributions for 1994 are plotted in cumulative form in Figures B2 and B3. Data for 1980 through 1994 are plotted in Figure B4.

Peak Spectral Wave Period Distributions

Annual and monthly peak wave period T_p distribution histograms for 1994 are presented in Figures B5 and B6. Data for 1980 through 1994 are presented in Figure B7.

Persistence of Wave Heights

Table B5 shows the number of times in 1994 when the specified wave height was equaled or exceeded at least once during each day for the duration (consecutive days). Data for 1980 through 1994 are averaged and given in Table B6. An example is shown below:

Height							Cons	ecut	ive	Day(s) or	Lon	nger						
 0.5	1	_2	_3	4	5	_6	7	_8	9	<u>10</u>	11	12	<u>13</u>	14	<u>15</u>	<u>16</u>	<u>17</u>	18	19+
0.5	18	15		14	13	12		11	10	9				8		7			
1.0	50	34	24	21	18	14	12	8	7	3			2						
1.5	41	19	8	6	2	1													
2.0	22	9	5	1															
2.5	10	5	2																
3.0	6	1																	
3.5		1																	
4.0	1																		

This example indicates that wave heights equaled or exceeded 1.0 m 50 times for at least 1 day; 34 times for at least 2 days; 24 times for at least 3 days, etc. Therefore, on 16 occasions the height equaled or exceeded 1.0 m for 1 day exactly (50 - 34 = 16); on 10 occasions for 2 days; on 3 occasions for 3 days, etc. Note that the height exceeded 1 m 50 times for 1 day or longer, while heights exceeded 0.5 m only 18 times for this same duration. This change in durations occurred because the longer durations of lower waves may be interspersed with shorter, but more frequent, intervals of higher waves. For example, one of the times that the wave heights exceeded 0.5 m for 16 days may have represented three times the height exceeded 1 m for shorter durations.

Spectra

Monthly spectra for the offshore Waverider buoy (Gauge 630) are presented in Figure B8. The plots show "relative" energy density as a function of wave frequency. These figures summarize the large number of spectra for each month. The figures emphasize the higher energy density associated with storms, as well as the general shifts in energy density to different frequencies.

As used here, "relative" indicates the spectra have been smoothed by the three-dimensional surface drawing routine. Consequently, extremely high-and low-energy density values are modified to produce a smooth surface. The figures are not intended for quantitative measurements; however, they do provide the energy density as a function of frequency relative to the other spectra for the month.

Monthly and annual wave statistics for Gauge 630 for 1994 and for 1980 through 1994 are presented in Table B7.

Figure B9 plots monthly time histories of wave height and period.

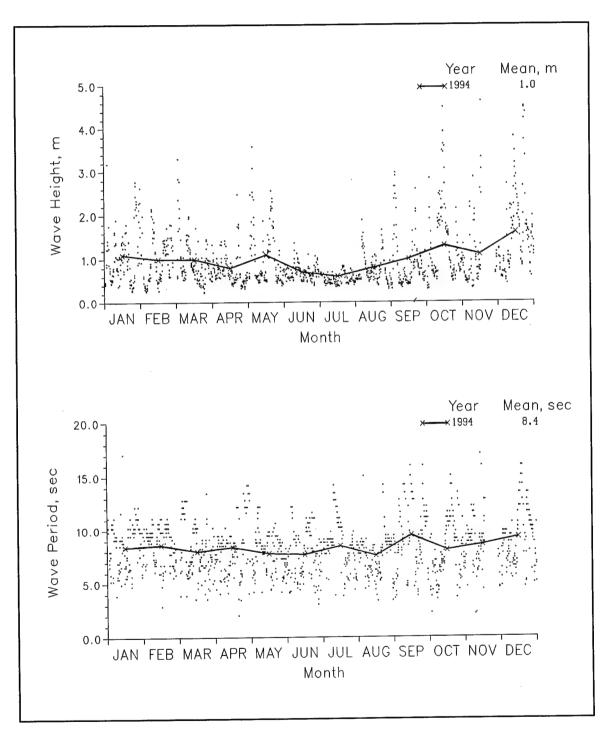


Figure B1. 1994 daily wave height and period values with monthly means for Gauge 630

Table B1 Annual Joint Distribution of H_{mo} versus T_p

			P	ercent	Occur 0	nnual rence()	1994, x100)	Gauge (of Heig	630 ght and	d Perio	od		
Height(m)						Pe	riod(s	ec)					Total
	2.0-	3.0- 3.9	4.0-		6.0- 6.9	7.0- 7.9	8.0- 8.9	9.0-	10.0- 11.9	12.0- 13.9	14.0- _15.9	16.0- Longer	
0.00 - 0.49 0.50 - 0.99 1.00 - 1.49 1.50 - 1.99 2.00 - 2.49 2.50 - 2.99 3.50 - 3.49 3.50 - 3.49 4.00 - 4.49 4.50 - 4.99	29 7	14 108 22	22 359 151	65 502 395 172 14	43 667 237 273 143 14	115 617 151 115 86 50 7	459 1055 187 57 36 36 7	416 861 158 36 29 22 14 22	244 581 194 136 50 22 50 22 7	158 57 22 29 7 7 7	108 273 57 57 50 36	14	1673 5101 1574 875 415 187 85 44 28
5.00 - Greater Total	36	144	532	1148	1377	1141	1837	1558	1306	30i	14 7 609	14	14 7

Table B2 Monthly Joint	Distri	butio	n of	H _{mo}	versı	ıs T _p	,						
			Pe	rcent	Occurr	Januar ence(X	y 1994 (100)	, Gaug	e 630 ht and	l Perio	d		
Height(m)							iod(se						Total
•	2.0-	3.0- 3.9	4.0- 4.9	5.0- 5.9	6.0-	7.0- 7.9	8.0- 8.9	9.0- 9.9	10.0- 11.9	12.0- 13.9	14.0- 15.9	16.0- Longer	
0.00 - 0.49 0.50 - 0.99 1.00 - 1.49 1.50 - 1.99 2.00 - 2.49 2.50 - 2.99 3.50 - 3.49 3.50 - 3.99 4.00 - 4.49 4.50 - 4.99 5.00 - Greater Total		82	82 82 82 	410 820 164 82	246 656 656 82	164 246 82 164 82 164 82 82	82 410 410 82	738 1148 246 82 82 82 	902 820 164 82 246 82		82	82	1804 3444 2624 1066 738 246 82 0 0
Height(m)					0ccur	rence() Pe	(100) riod(s	of Hei		d Perio			Total
	2.0-	3.0- 3.9	4.0-	5.0- 5.9	6.0- 6.9	7.0-	8.0- 8.9	9.0- 9.9	10.0- 11.9	12.0- 13.9	14.0- 15.9	16.0- Longer	
0.00 - 0.49 0.50 - 0.99 1.00 - 1.49 1.50 - 1.99 2.00 - 2.49	92	:	92 :	367 92 92 92	92 459 183 734 275	275 275 183 92	92 642 275 92	1284 1101 734 275	183 917 1101	:	:		1743 3853 2660 1376 367
2.50 - 2.99 3.00 - 3.49	:		:	:	:		:	:	:	:	:		0 0
3.50 - 3.99 4.00 - 4.49	:	:	:	:	:	:		:				:	0
4.50 - 4.99 5.00 - Greater Total	92	ö	92	551	1743	825	1101	3394	2201	ò	ö	ō	0
Height(m)	2.0-	3.0-	4.0-	5.0-	6 N-	rence(X100) eriod(s	of Hei sec)	10.0-	12.0-	14.0-	16.0- Longer	Total
0.00 - 0.49 0.50 - 0.99 1.00 - 1.49 1.50 - 1.99 2.00 - 2.49 2.50 - 2.99 3.00 - 3.49 3.50 - 3.99 4.00 - 4.49 4.50 - 4.99 5.00 - Greater Total		81 81 163 	244 163	81 569 244 81	163 894 732 325 	81 1220 325 163 81	325 650 163	163 407 163	163 1057 244 81	81	325 81 81 81 81 		1138 5447 2278 731 162 162 81 0 0
						(0	ontinu	ed)				(S	heet 1 of 4)

			P	ercent	0ccur	rence(X100)	4, Gaug of Heig	ge 630 ght and	d Perio	od		
Height(m)	2.0-	3.0- 3.9	4.0-	5.0-	6.0-	7.0-	8.0-	9.0-	10.0-	12.0-	14.0-	16.0-	Tota
0.00 - 0.49	2.9		4.9	5.9	_ 6.9	7.9	<u>8.9</u> 593	9.9	11.9 85	13.9 424	15.9 678	Longer	1780
0.50 - 0.99 1.00 - 1.49	85	85 85	339 169	593 678	678 85	932 254	1780 169	932	254	254	424	:	6356 1440
1.50 - 1.99 2.00 - 2.49		•		339			•	:	:	:	:	:	339
2.50 - 2.99		•	•	:	85	:		:	•	:	:	•	85
3.00 - 3.49 3.50 - 3.99	•		•	•			•			:	:		0
4.00 - 4.49		:	•		:	:	:	:	:	:		•	Č C C
4.50 - 4.99 5.00 - Greater	•	•	•	•	•		•	•	•	•			č
Total	85	170	508	1610	848	1186	2542	932	339	678	1102	ō	·
Height(m)			Pe	ercent	0ccur	rence()	ay 1994 (100) (4, Gaug of Heig ec)	ge 630 ght and	l Perio	od 		Tota
	2.0-	3.0- 3.9		5.0- 5.9	6.0-	7.0- 	8.0- 8.9	9.0- 9.9	10.0- 11.9	12.0- 13.9	14.0- 15.9	16.0- Longer	
0.00 - 0.49					242	323	403	161					1129
0.50 - 0.99 1.00 - 1.49	•	•	161 323	565	484	565	1774	968	161		242	:	4920
1.50 - 1 99	:		323	726 323	161 161	323	161 81	323 81	81 81	•	81	•	185 <i>6</i> 1050
2.00 - 2.49 2.50 - 2.99	•	:	•	•	242	81 161	161	161	81		•	•	726
3.00 - 3.49 3.50 - 3.99	:		:	:	:		81		:	:	:	•	161 81
4.00 - 4.49	:	:		:	•	•	•	81	•	•	•	•	81 0
4.50 - 4.99 5.00 - Greater	•		•	•				:	:	:	:	:	Õ
Total	Ö.	ō	484	1614	1290	1453	2661	1775	404	ò	323	ö	U
			Pe	ercent	0ccuri	Jur rence()	ne 1994 (100) (, Gaug	e 630 ht and	l Perio	od		
Height(m)			-			Per	iod(se	ec)					Tota
	2.0- 	3.0- 3.9	4.0- 4.9	5.0- 5.9	6.0- 6.9	<u>7.9</u>	8.0- <u>8.9</u>	9.0- 9.9	10.0- 11.9	12.0- 13.9	14.0- 15.9	16.0- Longer	
0.00 - 0.49 0.50 - 0.99	•	168	1008	1092	1345	252 840	504 1345	84 1092	252 1008		336		1092
1.00 - 1.49	:		168	420		040	84					:	8234 672
1.50 - 1.99 2.00 - 2.49	:		•	•	•	•	•	•	•	•	•	•	0
2.50 - 2.99 3.00 - 3.49	:	:	:	:	:	:	:	:	:			:	Ó
3.50 - 3.99	:	:	:	:	•							•	0
4.00 - 4.49 4.50 - 4.99		•	•	•	•	•	•	•	•				0
.00 - Greater	ö	168	:		•							Ö	0
Total			1176	1512	1345	1092	1933	1176	1260	0	336	^	-

			Pe	ercent	0ccurr	Jul ()ence	y 1994 (100) d	, Gaug of Heig	je 630 jht and	l Perio	nd		
Height(m)						Per	iod(se	ec)					_ Tota
	2.0-	3.0- 3.9	4.0- 4.9	5.0- 5.9	6.0-	7.0- 7.9	8.0- <u>8.9</u>	9.0- 9.9	10.0- 11.9	12.0- 13.9	14.0- 15.9	16.0- Longer	·
0.00 - 0.49	•	172	172 172	259 948	517	517 862	1638 1121	776 603	1121 172	345	86 517	•	4914 5084
0.50 - 0.99 1.00 - 1.49		1/2	1/2	940	•	•				:	•	:	0
1.50 - 1.99 2.00 - 2.49	:	:	:	:	•		:	:	:			:	0
2.50 - 2.99		•	•	•	•	•	•	•	•	•	•	•	0
3.00 - 3.49 3.50 - 3.99	:			:	:	•	:	:		:	:		0
4.00 - 4.49 4.50 - 4.99	•	•	•	•	•	•	•	:	•	•	:		0
5.00 - Greater	•	:	:	:	:			4770	1293	345	603	ō	0
Total	0	172	344	1207	517	1379	2759	1379	1273	342	003	v	
			P	ercent	0ccuri	rence()	(100)		ge 630 ght and	d Perio	od		
Height(m)							riod(s						_ Tota
	2.0-	3.0-	4.0- 4.9	5.0- 5.9	6.0-	7.0-	8.0-	9.0-	10.0-	12.0-	14.0-	16.0- Longe	r
	2.9	3.9	4.9		6.9	1.9			11.7	13.7	13.7	Longe	
.00 - 0.49 .50 - 0.99	•	248	413	331 744	1322	661	744 2645	248 413	:	248	83		1323 6777
1.00 - 1.49	:		165	413	83	248	248	248	83		•	•	1488 414
1.50 - 1.99 2.00 - 2.49	•	:	:	83	83	83	:	:	165	:	:	:	C
2.50 - 2.99	•			•	•	•			•	•	•	•	0
3.00 - 3.49 3.50 - 3.99	:	:	:	:	:	:	:			:	:	:	· d
4.00 - 4.49 4.50 - 4.99	•	•		•	•	•	•	•	:	:	:	• 1	0
5.00 - Greater Total	ö	248	578	1571	1488	992	3637	909	248	248	83	ó	С
				ı	S	eptemb	er 199	4, Gau	ge 630				
			P	ercent	0ccur	rence(X100)	of Hei	ght an	d Peri	od		T
Height(m)		7.0		F 0	6.0-		riod(s		10 0-	12 0-	1/. 0-	16 0-	Tota
	2.0-	3.9	4.9	5.9	6.9	7.9	8.9	9.9	11.9	13.9	15.9	Longe	
0.00 - 0.49		83	447	167	333	167 333	583 417	417 417	83 1333	1000	417 750		2750 4584
0.50 - 0.99 1.00 - 1.49	:	167	667 83	333 333	83	83	167	417	167	83	250	:	1249
1.50 - 1.99 2.00 - 2.49		•	•		167	83	83	83	83	:	83 83	:	499 499
2.50 - 2.49 2.50 - 2.99 3.00 - 3.49	:	:	:	:		83	250	83	•		•	•	416
3.50 - 3.99	•	:	:	:			:	:	:		:		((
4.00 - 4.49			•	•	•	•	•	•	•	•	•	•	(
4.50 - 4.99 5.00 - Greater	•	:	:				4500	4000	4//;	1007	1507	Ö	í
Total	ö	250	750	833	583	749	1500	1000	1666	1083	1583	U	

			P	ercent	t Occu	Octo rrence	ber 19 (X100)	94, Gau of Hei	ige 630 ght an	d Peri	od		
Height(m)							eriod(:			····			Tota
	2.0- 	3.0- 	4.0- <u>4.9</u>	5.0- 5.9	6.0- 2 <u>6.9</u>	7.0-	8.0- 8.9	9.0-	10.0- 11.9	12.0- 13.9	14.0- 15.9	16.0- Longer	
0.00 - 0.49 0.50 - 0.99	81	242	81 887	242	968	484	484	403 565	484	161	242	•	56
1.00 - 1.49 1.50 - 1.99		- :	161	323 323	161 484	81 81	161			161	81	•	4759 968
2.00 - 2.49 2.50 - 2.99	:	:	:	323	484	161	81	:	645 161	81	161	•	1936 88
3.00 - 3.49 3.50 - 3.99	:		:	•	81	81	81	81	81 161	:		•	324 242
4.00 - 4.49	:	:	:	:	:	:	:	81	161 81	•	•	•	247
4.50 - 4.99 5.00 - Greater	•	•	•				:	:	•		:	:	81
Total	81	242	1129	888	2178	888	807	1130	1774	403	484	ó	(
			P	ercent	0ccur	Novemb	per 199 (X100)	4, Gau of Hei	ge 630 ght and	d Perio	od		
Height(m)							riod(s						Tota
	2.0-	3.0-	4.0-	5.0-	6.0-	7.0-	8.0-	9.0-	10.0-	12.0-	14.0-	16.0- Longer	
0.00 - 0.49	267			133						13.9	15.9	Longer	
0.00 - 0.49 0.50 - 0.99		:	133	133	400	667	533 933	933 1600	133 533		267	133	1999 4666
1.00 - 1.49 1.50 - 1.99 2.00 - 2.49 2.50 - 2.99	•	:	400	133	267 267	133 267	267	133	:	:	133		1466 534
.50 - 2.99	•	:	•	133	267	267	133	•	•	•	•	•	533 267
3.50 - 3.49 3.50 - 3.99	:	:	•	•	•	•	•	•	267	:		:	267
.00 - 4.49 .50 - 4.99	• ,	•	•		:	:	:	:	:	:	475	:	0
.00 - Greater Total	267	ö	533	399	1201	477	•	:	:	•	133 133	:	133 133
	201	v		3,,,		1334	1866	2666	933	0	666	133	
Height(m)		,		ercent	Occur	rence(er 1996 X100) riod(se		ge 630 ght and	Perio	d		ľota
	2.0-	3.0- 3.9	4.0- 4.9	5.0- 5.9	6.0- 6.9	7.0-	8.0-	9-0-	10.0-	12.0- 13.9	14.0-	16.0- Longer	1014
.00 - 0.49	•					_	81	81				201.301	162
.50 - 0.99 .00 - 1.49 .50 - 1.99	•	•	163	163 407	244 407	407 163	407 325	1382 81	244 488	:	81 81		2928
.00 - 2.49	•	:	•	244	569	244	244		488	244	81 325	:	2115 2358
.50 - 2.99 .00 - 3.49	:	:	:		163 81	325		163	81	81 81	407 244	:	976 650
.50 - 3.99	:	:	:	:		:	:	81 81	163 81	81	•	•	325 162
.00 - 4.49 .50 - 4.99	•	:		•	•	•	•	•	•	163	81 81	•	244
.00 - Greater Total	ö	ó	163	814	1464	1139	1057	1860	15/5	450			81 0
. • • • • • • • • • • • • • • • • • • •	U	J	103	014	1404	1139	1057	1869	1545	650	1300	0	

Table B3 Annual Joint Distribution of H_{mo} versus T_p (All Years)

Height(m)			Pe	ercent	Occur!	rence(1980- (100) (of Heig	Gauge (ght and	630 d Perio	od		Total
	2.0-	3.0- 3.9	4.0- 4.9	5.0- 5.9		7.0- 7.9	8.0- 8.9	9.0- 9.9		12.0- 13.9		16.0- Longer	
0.00 - 0.49 0.50 - 0.99 1.00 - 1.49 1.50 - 1.99 2.00 - 2.49 2.50 - 2.99 3.00 - 3.49 3.50 - 3.99 4.00 - 4.49 4.50 - 4.99 5.00 - Greater Total	25 32	15 135 10 	28 271 147 11 1 	63 490 405 166 25 1	80 570 404 244 93 14 1	123 536 237 106 68 34 11 1	356 915 274 82 52 20 13 6 3	293 773 216 76 333 15 13 9 5 1	194 764 318 137 62 34 21 13 8 2 1 1554	68 125 39 32 26 9 6 5 3	119 225 112 66 34 25 8 5 4 1 1 600	14 33 1 1 1 1 1 30	1368 4850 2165 923 395 153 74 39 24 5

Height(m)	January 1980-1994, Gauge 630 Percent Occurrence(X100) of Height and Period Period(sec)	
	2.0- 3.0- 4.0- 5.0- 6.0- 7.0- 8.0- 9.0- 10.0- 12.0- 14.0- 16.0- 2.9 3.9 4.9 5.9 6.9 7.9 8.9 9.9 11.9 13.9 15.9 Longer	Tota
0.00 - 0.49 0.50 - 0.99 1.00 - 1.49 1.50 - 1.99 2.00 - 2.49 2.50 - 2.99 3.00 - 3.49 3.50 - 3.99 4.00 - 4.49 4.50 - 4.99 5.00 - Greater Total	80 7 7 67 60 33 134 294 254 40 94 60 180 201 388 368 321 408 749 809 87 187 7 60 180 201 388 368 321 408 749 809 87 187 7 60 180 201 388 368 321 408 749 809 87 187 7 60 180 201 388 368 321 408 749 809 87 187 7 60 180 201 388 368 321 408 749 809 87 187 7 60 180 201 388 368 321 408 749 809 87 187 7 60 180 200 401 180 87 107 214 33 47 61 107 214 31 47 61 107 214 31 61	1070 3765 2614 1437 681 307 94 20 7
Keight(m)	February 1980-1994, Gauge 630 Percent Occurrence(X100) of Height and Period Period(sec)	Tota
Height(m)	2.0- 3.0- 4.0- 5.0- 6.0- 7.0- 8.0- 9.0- 10.0- 12.0- 14.0- 16.0- 2.9 3.9 4.9 5.9 6.9 7.9 8.9 9.9 11.9 13.9 15.9 Longer	1014
0.00 - 0.49 0.50 - 0.99 1.00 - 1.49 1.50 - 1.99 2.00 - 2.49 2.50 - 2.99 3.00 - 3.49 3.50 - 3.99 4.00 - 4.49 4.50 - 4.99 5.00 - Greater	15	627 3876 3048 1346 622 295 111 21 44 0
Height(m)	March 1980-1994, Gauge 630 Percent Occurrence(X100) of Height and Period Period(sec)	Total
	2.0- 3.0- 4.0- 5.0- 6.0- 7.0- 8.0- 9.0- 10.0- 12.0- 14.0- 16.0- 2.9 3.9 4.9 5.9 6.9 7.9 8.9 9.9 11.9 13.9 15.9 Longer	
.00 - 0.49 .50 - 0.99 .00 - 1.49 .50 - 1.99 .00 - 2.49 .50 - 2.99 .00 - 3.99 .00 - 4.49 .50 - 4.99 .00 - Greater Total	6 12 6 18 41 47 136 53 171 59 101 . 12 71 195 402 497 479 603 627 887 95 231 18 213 420 514 308 319 278 651 53 278 12 219 260 112 95 130 266 59 112	650 4099 3052 1265 503 190 95 83 54

			Pe	ercent	Occurr	April ence(X	1980-1 100) d	994, 0 f Heig	auge 6 ht and	30 Perio	d		
Height(m)							iod(se						Total
	2.0-	3.0- 3.9	4.0- 4.9	5.0- 5.9	6.0-	7.0- 7.9	8.0- 8.9	9.0- 9.9	10.0- 11.9	12.0- 13.9	14.0- 15.9	16.0- Longer	
.00 - 0.49 .50 - 0.99 .00 - 1.49 .50 - 1.99 .50 - 2.99 .50 - 3.49 .50 - 3.99 .00 - 4.49 .50 - 4.99 .00 - Greater Total	6 72	12 174 12 	18 228 108 6	36 479 293 168 30 6	30 599 353 132 66 18	24 509 311 72 24 18 24 6	257 904 341 84 42 30 12 24 6	162 814 311 84 48 18 24 6	126 1006 329 186	96 234 66 18 24 24 6	138 383 120 66 6 12		905 5402 2244 816 324 168 90 36 12 6
Height(m)			Р	ercent	Occur	rence()	1980- (100) -iod(s	of Heig	Sauge 6	30 d Perio	od		Tota
	2.0-	3.0- 3.9	4.0- 4.9	5.0-	6.0-	7.0- 7.9	8.0- 8.9	9.0- 9.9	10.0- 11.9	12.0- 13.9	14.0- 15.9	16.0- Longer	-
0.00 - 0.49 0.50 - 0.99 0.00 - 1.49 1.50 - 1.99 0.00 - 2.49 0.00 - 3.49 0.00 - 3.49 0.00 - 3.49 0.00 - 4.49 0.00 - 4.99 0.00 - Greater	6 18	18 187 6	41 362 169 6	88 560 251 88 12	140 531 292 88 64 23	146 788 169 64 53 18	356 1255 356 105 23 6 18	298 1010 263 76 41 6 6 6	198 677 269 111 12 6 6 6	64 88 12 18 18 12 6	128 204 76 47 18 6 6	6	1483 5686 1863 603 241 77 42 12 0 0
Height(m)			P	ercent	Occur	rence(1980- x100) riod(s	of Hei	Gauge ght an	630 d Peri	od		Tota
		3.0- 3.9		5.0-	6.0-	7.0- 	8.0-	9.0-	10.0- 11.9	12.0- 13.9	14.0- 15.9	16.0- Longer	
0.00 - 0.49 0.50 - 0.99 1.00 - 1.49 1.50 - 1.99 2.00 - 2.49 2.50 - 2.99 3.00 - 3.49 3.50 - 3.99 4.00 - 4.49 4.50 - 4.99 5.00 - Greater	19 38	25 188 6 	38 394 113 13 	100 651 257 44 - - - 1052	163 808 207 81 19	301 783 163 44 13 6	639 1653 182 25 38	482 1033 81 13 6	276 564 81 75	31 125	25 131 31 38		2099 6368 1121 333 76 0 0 0

Unight/m)			P	ercent	0ccur	rence(X100)	1994, (of Heig	Gauge (ght and	330 d Perio	od		. .
Height(m)	2.0-	3.0- 3.9	4.0-	5.0-	6.0-	7.0-	<u>riod(s</u> 8.0- 8.9	9.0-	10.0-	12.0-	14.0- 15.9	16.0- Longer	Tota
0.00 - 0.49	12	18 184	74 374	147 700	196 798	424 737	1197 1320	755 915	325 356	98	172 135	12 49	3430 5765
1.00 - 1.49 1.50 - 1.99	:	12	49	166 37	203	74 12	104	31 12	31 31	•		•	670 116
2.00 - 2.49 2.50 - 2.99	:	:	:	6	·		6		•	:	:	:	12
.00 - 3.49 .50 - 3.99	:	:		:	:	:	:	:	•	:	:	•	0
00 - 4.49	:	:	:	:			:			•	•	:	0
.50 - 4.99 .00 - Greater						•	•	•	:			:	0
Total	43	214	497	1056	1203	1247	2645	1713	743	264	307	61	
11.5.1.4.3			P	ercent	Occur	rence(X100)	1994, (of Heig	Sauge 6 ght and	30 I Perio	od		
leight(m)	2.0-	3.0-		5.0-	6.0-	7.0-	8.0-	9.0-	10.0-	12.0-	14.0-	16.0-	Tota
	2.9	3.9	4.9	5.9								Longer	
).00 - 0.49).50 - 0.99	18 30	12 <u>1</u>	60 284	115 550	139 822	193 798	616 1456	465 840	284 719	60 145	79 254	30	2053 6049
.00 - 1.49 .50 - 1.99	:	6	127	302 66	260 115	193 48	236 24	139 12	91 42	12 6	30 30		1396 337
1.00 - 2.49 1.50 - 2.99	:	•	:	12	24 6	12	12 12	:	24 12	6	6		96 3 6
.00 - 3.49 .50 - 3.99	:	:	:	:	6	6	6	ć	6	:	•	:	24
.00 - 4.49 .50 - 4.99	:	•	:	:	:		:		:	:	•		Õ
.00 - Greater Total	48	151	471	1045	1372	1250	2362	1462	1178	223	405	30	ŏ
	·		Pe	ercent	Sep ¹ Occuri	tember rence()	1980~1 (100)	1994, 0 of Heig	lauge 6	30 Perio	d		
Height(m)							iod(s						Tota
	2.0-	3.0- 3.9	4.0- 4.9	5.0- 5.9	6.0- <u>6.9</u>	7.0- 7.9	8.0- <u>8.9</u>	9.0- <u>9.9</u>		12.0- 13.9	14.0- 15.9	16.0- Longer	
.00 - 0.49 .50 - 0.99	6	12 121	18 242	30 387	30 484	67 568	230 955	248 786	181 979	157 121	103 290	6	1088 4933
.00 - 1.49 .50 - 1.99		121	242 79 12	387 459 151	484 453 254	284	955 435 79	224 97 24	302 60	121 79 18	145 91	6	2478 883
.00 - 2.49 .50 - 2.99	•	:	:	30	85	115 48 54	60 36	24 12	54	48	54 6	•	403 120
.00 - 3.49 .50 - 3.99	:	•	:	:	:	6	12	6	6	6	6	:	42
.00 - 4.49 .50 - 4.99	:	:	:	:	:	:	š	•	6		•	•	42 30 12
.00 - Greater Total	6	145	35i	1057	1306	1142	1819	1403	1600	6 447	701	18	0 6

			Pe	ercent	Occur	ctober rence()	1980- (100)	1994, (of Hei	Gauge (ght an	630 d Perio	od		
Height(m)	2.0-		17 174 607 359 168 208 254 393 87 191 . 23 237 393 127 98 87 202 87 174 23 . . . 29 139 156 87 64 139 35 52 6 <th>Tota</th>				Tota						
0.00 - 0.49 0.50 - 0.99 1.00 - 1.49 1.50 - 1.99 2.00 - 2.49 2.50 - 2.99 3.00 - 3.49 3.50 - 3.99 4.00 - 4.49 4.50 - 4.99 5.00 - Greater Total	29 23 	69 17	6 220 174 23	6 341 607 237 29	35 393 359 393 139 35	64 341 168 127 156 87 23	185 746 208 98 87 35 6 12	139 526 254 87 64 52 12 29 17	191 827 393 202 139 52 29 17	23 174 87 87 35 17 12	121 330 191 174 52 52 29 6	6 23 6 6 6 6 6 6	799 3996 2456 1457 707 333 1118 857
Height(m)			Po		0ccur	rence() Per	(100) riod(s	of Heig ec)	ght and	d Perio			Tota
	2.0- 2.9	3.0- 3.9	4.0- <u>4.9</u>	5.0- 	6.0- <u>6.9</u>	7.0- 7.9	8.0- <u>8.9</u>	9.0- 9.9	10.0- 11.9	12.0- 13.9	14.0- 	16.0- Longer	
0.00 - 0.49 0.50 - 0.99 1.50 - 1.49 1.50 - 1.99 2.00 - 2.49 2.50 - 2.99 3.00 - 3.49 3.50 - 3.99 4.00 - 4.49 4.50 - 4.99 5.00 - Greater Total	48 34	27 95 14	20 327 259 14	34 565 476 224 34	41 510 633 361 150 7	82 463 395 197 109 41 7	272 578 306 143 102 7 14 7	231 612 293 95 27 14 48 14 7 7	82 544 313 136 34 41 27 7	61 102 41 41 41 14 7 14 7 -	177 122 116 7 7 14 7 7 7 7	20 41 20 7	109' 399: 286 122' 47' 11' 12: 6' 2
00 - 3.49		Tot											
	2.0-	3.0- 3.9	4.0- 4.9	5.0- 5.9	6.0-	7.0-	8.0-	9.0-	10.0- 11.9	12.0- 13.9	14.0- 15.9	16.0- Longer	
0.00 - 0.49 0.50 - 0.99 1.00 - 1.49 1.50 - 1.99 2.00 - 2.49 2.50 - 2.99 3.00 - 3.49 4.00 - 3.49 4.50 - 4.99 5.00 - Greater	61 34	20 149	34 244 183 20 14	68 468 454 244 7	20 542 549 508 224 7	34 244 292 176 129 41 7	95 414 231 122 41 54 20	203 631 163 68 34 34 20 20 14	115 766 386 156 75 68 34 27 7	102 129 34 47 68 7 20 20 34 7 468	210 251 129 88 88 68 27 20 27 7 7 7 922	7 27	96' 389' 242' 142' 68' 22' 16' 10' 8

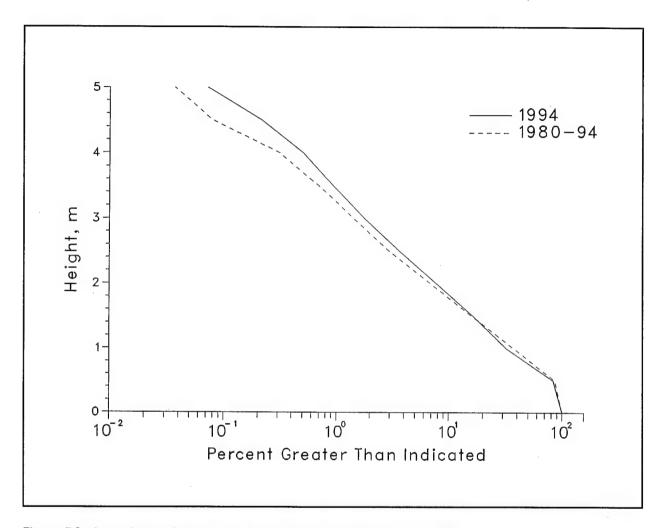


Figure B2. Annual cumulative wave height distributions for Gauge 630

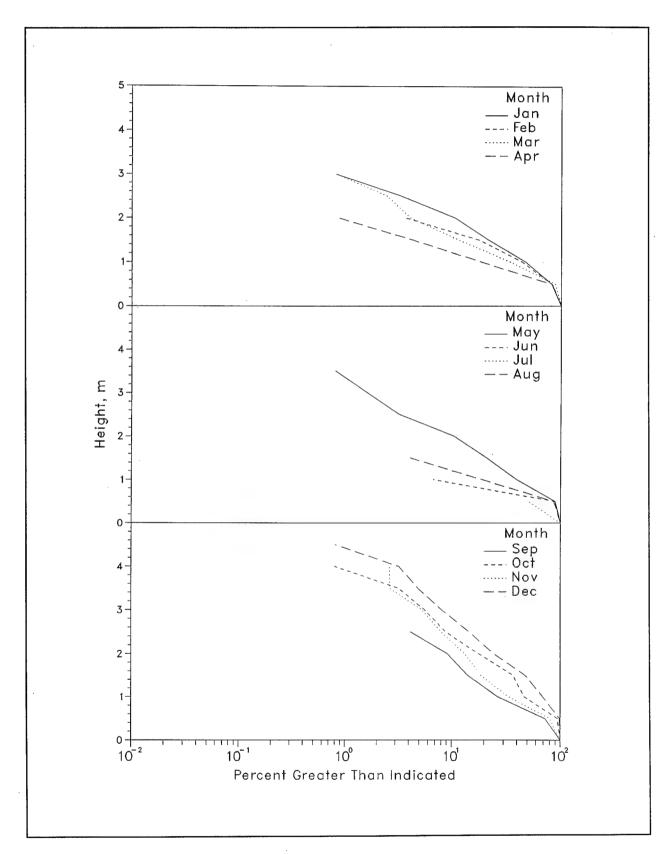


Figure B3. 1994 monthly wave height distributions for Gauge 630

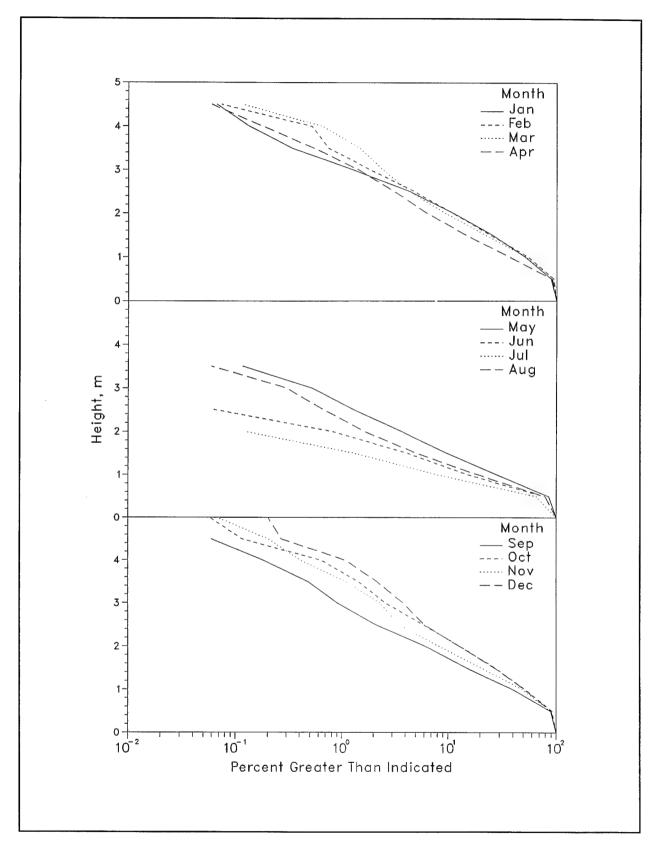


Figure B4. 1980-1994 monthly wave height distributions for Gauge 630

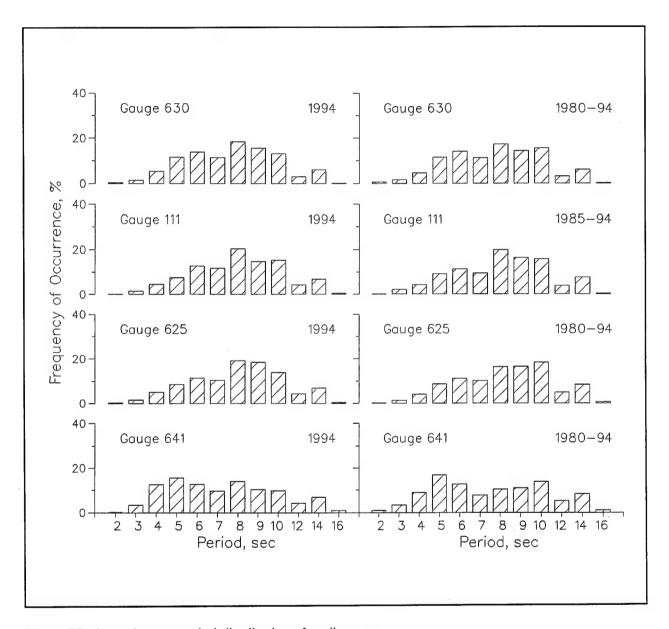


Figure B5. Annual wave period distributions for all gauges

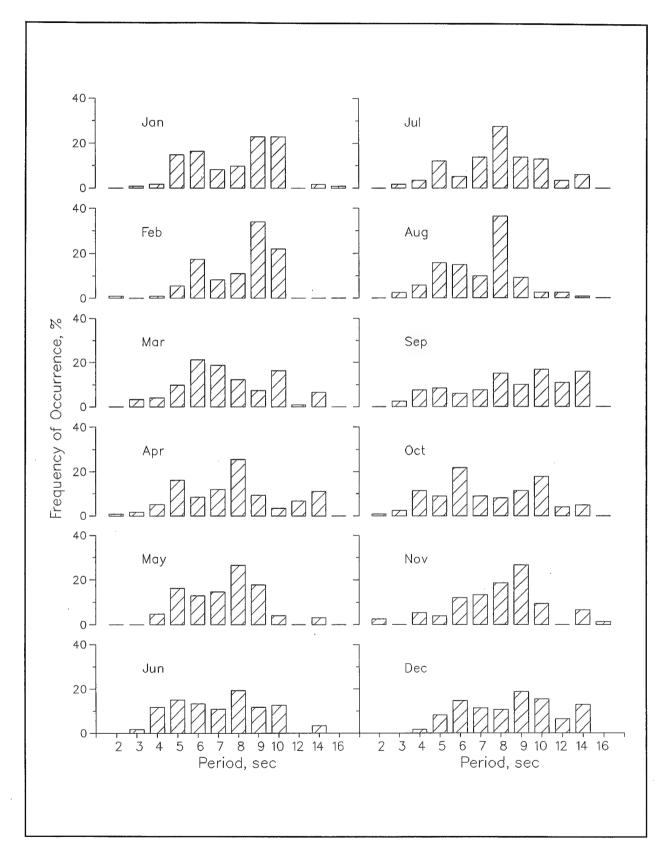


Figure B6. 1994 monthly wave period distributions for Gauge 630

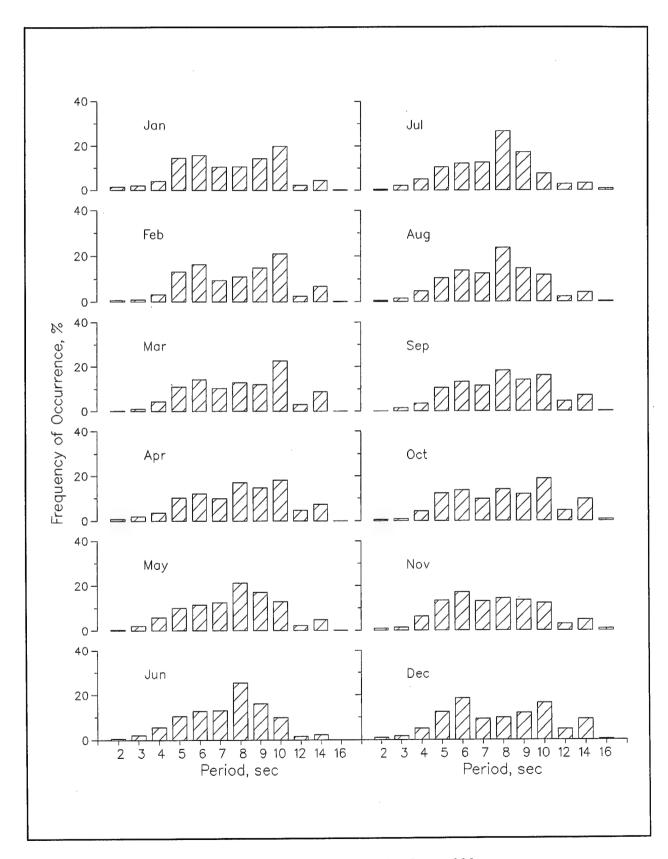


Figure B7. 1980-1994 monthly wave period distributions for Gauge 630

Table B5 1994 persistence of H_{mo} for Gauge 630

2 3 16 15 32 21 24 10 13 5	4 14 13 6 3	9	6 7 4	7 13 6	8 9	10	11 3	12 11	13	14	15 10	16	17	18	19-
32 21 24 10	13 6	-	7	13 6		1	3	11			10				9
24 10	6	-	7 4	6	5	1	3								-
	_	_	4			1									1
13 5	7	_													
	3	2	1												
6 4	1														
4 1															
3															
2															
4	1	1	1	1	1	i	1	1	1	1	1	i	1	1	1

Table B6 1980 through 1994 persistence of H_{mo} for Gauge 630

Height	Consecutive Day(s) or Longer																		
(m)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19-
0.5	19	18	16	14	13	12	11		10			9	8	7		6			5
1.0	50	34	24	17	14	10	8	6	5		3		2				1		
1.5	37	22	12	6	4		2		1										
2.0	22	11	5	2		1													
2.5	11	5	2																
3.0	6	3	1																
3.5	3	1																	
4.0	2	1																	

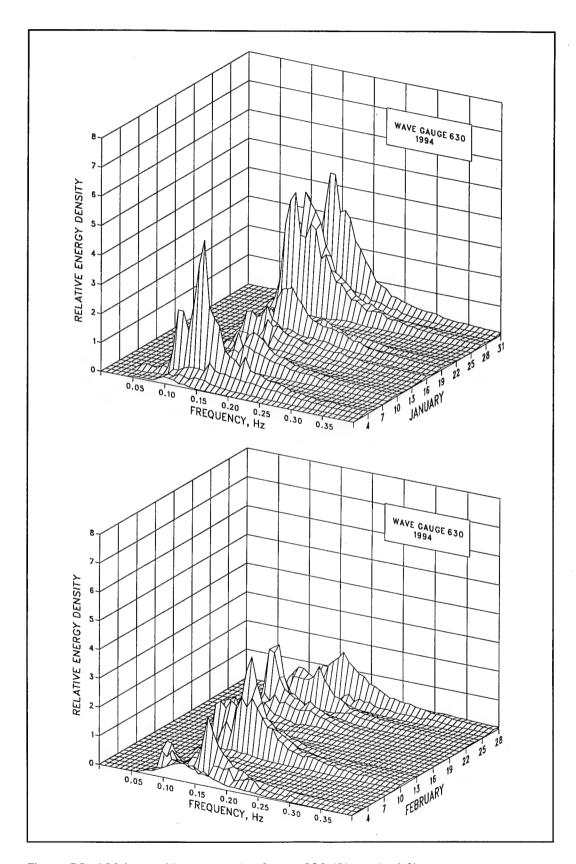


Figure B8. 1994 monthly spectra for Gauge 630 (Sheet 1 of 6)

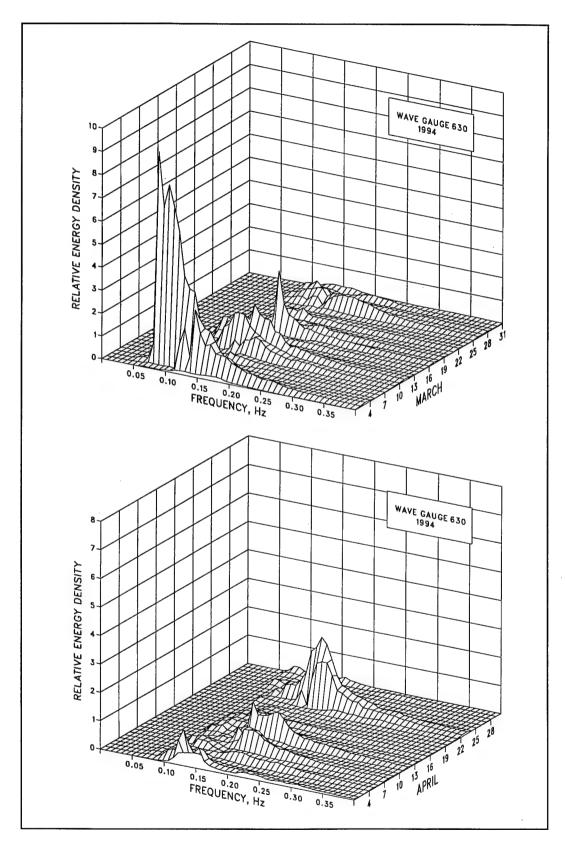


Figure B8. (Sheet 2 of 6)

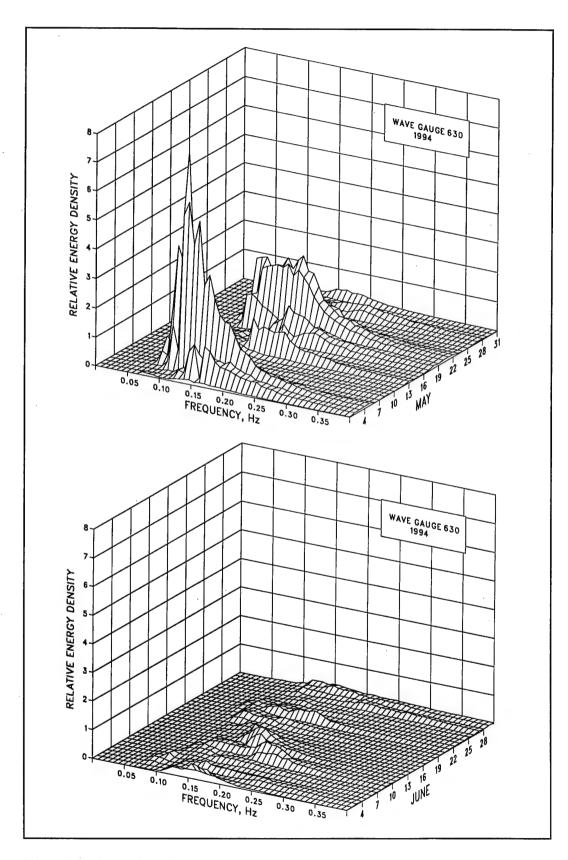


Figure B8. (Sheet 3 of 6)

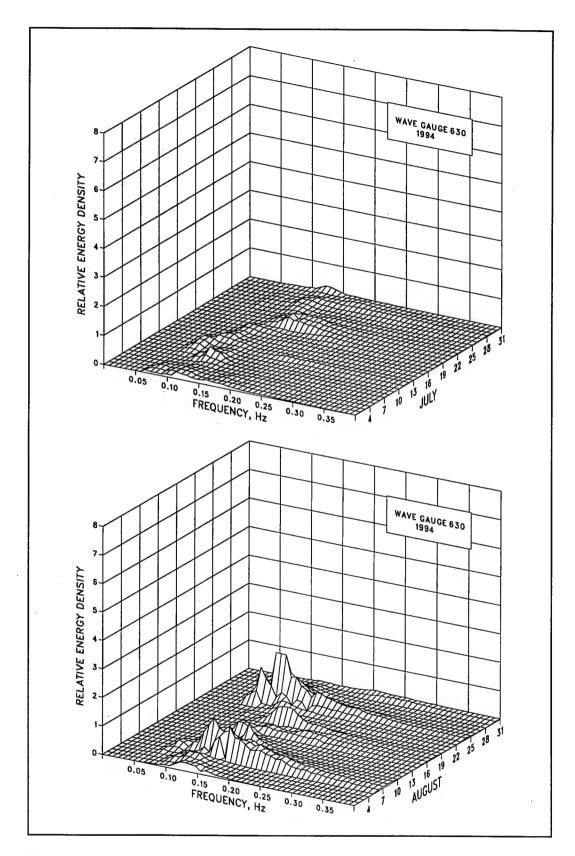


Figure B8. (Sheet 4 of 6)

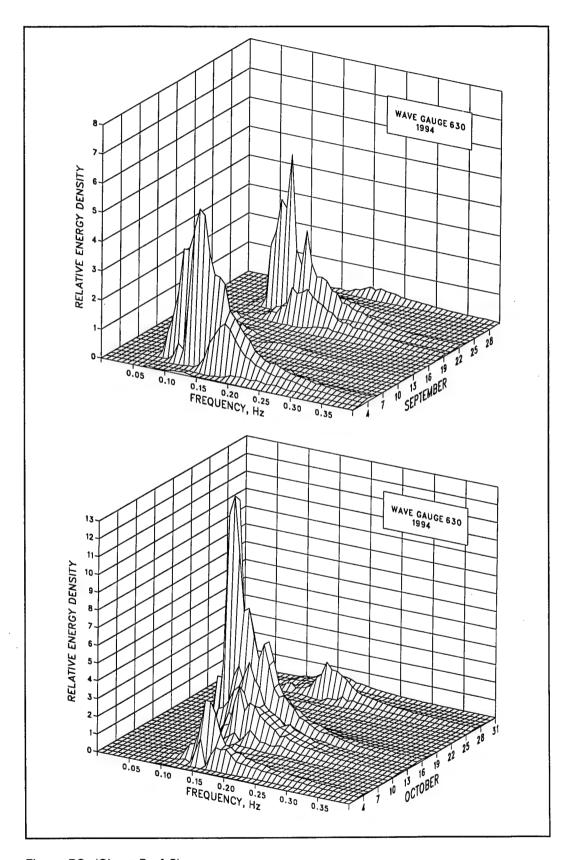


Figure B8. (Sheet 5 of 6)

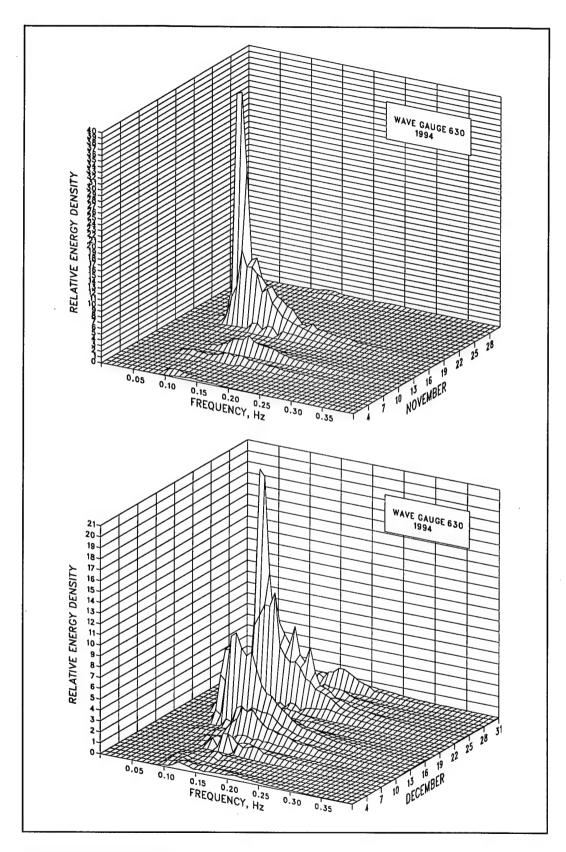


Figure B8. (Sheet 6 of 6)

Table B7
Wave statistics for Gauge 630

				1994						1	980-1994			
		He	ight		Period				Не	ight		Per		
	Std.			Std.					Std.				Std.	
	Mean	Dev.	Extreme		Mean	Dev.	Number	Mean	Dev.	Extreme	:	Mean	Dev.	Number
<u>Month</u>	_m_	_m_	m	<u>Date</u>	sec	sec	Obs.	<u>m</u>	<u>m</u>	m	Date	sec	sec	Obs.
Jan	1.1	0.7	3.2	3	8.4	2.2	122	1.2	0.7	4.5	1983	8.1	2.6	1496
Feb	1.0	0.6	2.2	10	8.6	1.8	109	1.2	0.7	5.1	1987	8.4	2.5	1352
Mar	1.0	0.6	3.3	2	8.0	2.4	123	1.2	0.7	4.7	1983	8.6	2.6	1691
Apr	0.8	0.4	2.5	22	8.4	2.7	118	1.0	0.6	5.0	1988	8.6	2.7	1670
May	1.1	0.7	3.6	4	7.8	1.9	124	0.9	0.5	3.6	1994	8.2	2.4	1713
Jun	0.7	0.2	1.4	9	7.7	2.3	119	0.8	0.4	2.7	1991	7.9	2.2	1597
Jul	0.6	0.2	0.8	20	8.5	2.3	116	0.7	0.3	2.1	1985	8.0	2.4	1629
Aug	0.8	0.4	1.9	6	7.6	2.1	121	0.8	0.4	3.6	1981	8.1	2.4	1655
Sep	1.0	0.7	3.0	4	9.5	3.2	120	1.0	0.6	6.1	1985	8.6	2.6	1654
Oct	1.3	0.9	4.5	15	8.1	2.9	124	1.3	0.8	5.4	1991	8.7	2.8	1729
Nov	1.1	1.0	5.1	18	8.6	2.6	75	1.2	0.7	5.1	1994	8.0	2.7	1470
Dec	1.6	1.0	4.5	23	9.3	2.8	123	1.3	0.8	5.6	1980	8.4	2.9	1475
nnual	1.0	0.7	5.1	Nov	8.4	2.5	1394	1.0	0.7	6.1	Sep 1985	8.3	2.6	19131

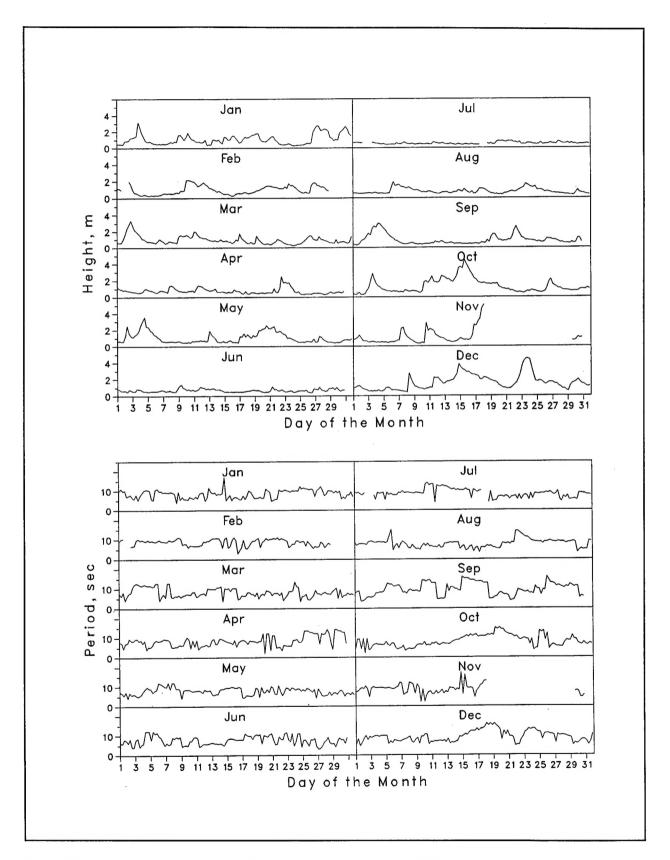


Figure B9. Time-histories of wave height and period for Gauge 630

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13. ABSTRACT (Maximum 200 words)

This report provides basic data and summaries for the measurements made during 1994 at the U.S. Army Engineer Waterways Experiment Station (WES), Coastal Engineering Research Center's (CERC's) Field Research Facility (FRF) in Duck, NC. The report includes comparisons of the present year's data with cumulative statistics from 1980 to the present.

Summarized in this report are meteorological and oceanographic data, monthly bathymetric survey results, samples of biannual aerial photography, and descriptions of 15 storms that occurred during the year. The year was highlighted by a major storm in mid-March which caused extensive flooding and damage on the western (soundside) side of the Outer Banks.

This report is the 16th in a series of annual summaries of data collected at the FRF that began with Miscellaneous Report-CERC-82-16, which summarizes data collected during 1977-1979. These reports are available from the WES Technical Report Distribution Section of the Information Technology Laboratory, Vicksburg, MS.

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